



UCC File: 5331

FUNCTIONAL SERVICING REPORT

Rosedale Subdivision City of Port Colborne November 2023

INTRODUCTION

Upper Canada Consultants has been retained to undertake and provide a Functional Servicing Report to address the servicing needs and requirements for the proposed residential development known as Rosedale Subdivision as part of the Draft Plan of Subdivision application process for the City of Port Colborne.

The project site is located in the City of Port Colborne as part of Lot 30 and Concession 3 and is situated south of Stonebridge Drive, west of Elm Street, with West Side Road (Highway 58) at the west site limits and at the north limit of Oxford Boulevard. The site is approximately 12.77 hectares and shall consist of 131 single family dwellings and 118 townhouse units for a total unit count of 249 units. A park block (Block 153) will be located at the south-east corner of the site and Block 154 at the north limits will consist of the proposed Stormwater Management (SWM) Facility.

Currently, separate engineering submission are being made for the easterly adjacent Meadow Heights (Phase 3) subdivision. It is expected that the Meadow Heights development will be completed prior to the Rosedale Subdivision and the servicing infrastructures from both developments will ultimately be connected. The site shall include associated asphalt road, concrete curb, catch basins, storm sewers, sanitary sewers, and watermain.

The objectives of this study are as follows:

1. Identify domestic and fire protection water service needs for the site;
2. Identify sanitary servicing needs for the site; and,
3. Identify stormwater management needs for the site.

WATER SERVICING

The following existing watermains are located in close proximity to the proposed development:

- 400mm diameter watermain on Stonebridge Drive
- 300mm diameter watermain on Meadowlark Drive
- 150mm diameter watermain on Oxford Boulevard



It is expected as part of the adjacent Meadow Heights Subdivision development, the 300mm diameter Meadowlark Drive watermain will be extended westerly on Meadowlark Drive to the new Parkside Drive and then continue northerly to the proposed Westfield Place at the north end of the site. This 300mm diameter watermain will then continue north, immediately adjacent to the Rosedale SWM facility, and ultimately connect to the Stonebridge Drive 400mm diameter watermain providing a loop.

The servicing plan for the proposed Rosedale Subdivision will result in watermain connections at the following locations to provide both domestic and fire water supply:

- 300mm diameter Meadowlark Drive watermain extended westerly from Meadow Heights
- 300mm diameter Westfield Place watermain
- 150mm diameter Oxford Boulevard watermain

Fire protection will be provided to the proposed development with municipal fire hydrants within the subdivision. The sizes and locations of the proposed internal watermain and hydrants will be finalized as part of the future detailed design. It is expected approximately 8 proposed municipal hydrants will be required on this site to adequately provide the necessary fire protection.

Upper Canada Consultants has undertaken a watermain analysis using the EPANET software to model flows and pressures within the existing and proposed system as a result of the proposed development under various conditions. The software was used to model the conditions utilizing average day, maximum day, and peak unit consumption rates per MECP standards. The model has been calibrated utilizing hydrant test flow data provided by the municipality from tests conducted in May/June of this year and have ensured supportable conclusions for this development.

As the adjacent Meadow Heights (Phase 3) subdivision has not yet been completed, this development has included both subdivisions within the modelling. The modelling utilizes the proposed watermains to be constructed as part of the proposed development plan for Meadow Heights Phase 3, and a preliminary watermain design for the proposed Rosedale Subdivision. It is proposed to extend the 300mm diameter Meadowlark Drive watermain to Street B in Rosedale Subdivision, and continue with a 150mm diameter for the remainder of the subdivision. Images detailing the proposed watermain design can be found in Appendix A. Elevations were used per the Rosedale Preliminary Grading Design page also included in Appendix A

The EPANET model has utilized flow test data from seven hydrants located at the following locations:

1. Apollo Drive at Oriole Crescent (Hyd #6300009)
2. Meadowlark Drive, 120m west of Elm Street (Hyd #63000020)
3. Fronting #59 Hillcrest Road (Hyd # 63000304)
4. Fronting #10 Oxford Boulevard (Hyd #63000157)
5. Fronting #20 Oxford Boulevard (Hyd #63000158)
6. Stonebridge Drive, 2nd hydrant east of Highway 58 (Hyd #63000160)
7. Stonebridge Drive, 2nd hydrant west of Petersburg Circle (Hyd #63000283)



The model was able to replicate the static and residual pressures in the above noted hydrants to within 5% of the values documented from in the City of Port Colbornes' hydrant testing results as shown on the calculation page in Appendix A. Different pressure zones were observed north and south of the proposed subdivision. Through the modelling, an increase of approximately 5% was noted to the static pressure at existing Oxford Boulevard hydrants while a decrease of approximately 2% was noted to the static pressures on Stonebridge Drive as the pressure equalizes with the new connections. However, this new looping is modelled to significantly increase the future calculated theoretical fire flows at 20PSI in all existing fire hydrants

Due to the extreme elevation differences on the site, the proposed hydrant located at the highest point at the intersection of Oxford Boulevard and Street 'C' will experience the lowest pressures (and therefore flows rates) through this modelling. The hydrant will provide a reduced flow rate of 150L/s at 20 PSI under peak day conditions. Per Table 8 of the 'Water Supply of Public Protection' guideline (Fire Underwriters Survey, 2020) regarding minimum required flow rates for row housing exposures, a minimum flow rate of 133.3L/s is required for townhouses experiencing exposure distances of 3 to 10m. As all townhouse structures on site are separated by approximately 3.1m, and the minimum provided fire flow is greater than 133.3L/s, the proposed watermain system is expected to provide sufficient fire flow for the development. Additionally, as shown in the Rosedale Subdivision Static Pressure imagery in Appendix A, all proposed hydrants within the system will provide static pressures within the preferred system range of 50-80 PSI (35.2-56.2 m of H₂O). Only the existing hydrant fronting #59 Hillcrest Road will remain slightly below at 45.4 PSI (higher than the 40PSI minimum standard), though this is an increase from existing conditions.

This model is limited in scope with regards to the impact of the City's system. Therefore, tolerances between this analysis and the City's overall model should prioritize results obtained from the large City model. It should be noted that the pressures and flow rates observed by this model are purely theoretical, attempting to replicate information provided by the City's hydrant flow test data for hydrants within the immediate vicinity of the proposed development site. Without a complete model of the city's entire water system, a highly accurate model providing reliable flow rate data for the future development is unobtainable.

SANITARY SERVICING

There is an existing 300mm diameter municipal sanitary sewer located on Stonebridge Drive conveying flows westerly before directing flows north-east along the south limit of the Biederman Municipal Drain. The sewer conveys flows easterly along the south limit of the Elm Street Lease Free Dog Park before discharging flows to the Industrial Park Sanitary Pumping Station.

As part of the adjacent Meadow Heights (Phase 3) subdivision, a 300mm diameter sanitary sewer will be constructed immediately east of the proposed Rosedale Subdivision Stormwater Management Facility, through a servicing easement on the Van Jon Paving property (#64 Stonebridge Drive), and discharge to a maintenance hole on Stonebridge Drive at the extreme upstream limit of the sanitary sewer. It is proposed to discharge sanitary flows from the proposed



Rosedale Subdivision to the 300mm diameter Meadow Heights easement sanitary sewer. This easement sanitary sewer has been designed to convey sanitary flows from the proposed Rosedale Subdivision development.

An overall sanitary analysis has been conducted and included in Appendix B for the municipal sanitary sewer system downstream of the proposed development site from the site connection to the Regional Sanitary Sewer at the Industrial Park Sanitary Pumping Station (SPS). The analysis utilizes a flow rate of 0.2 L/s/gross hectare as well as a Peak Factor of 2.0 for industrial lands north of the site as recommended in the 'Design Criteria for Sanitary Sewers, Storm Sewers and Forcemains for Alterations Authorized under an Environmental Compliance Approval' per the Ministry of the Environment, Conservation and Parks (MECP, 2023). Additionally, an Infiltration Rate of 0.28 L/s/ha is used with a Residential Flow rate of 255 L/cap/day per Regional '2021 Water and Wastewater Master Servicing Plan Update' (2023). All existing sanitary sewer information utilized in the analysis is per information provided by the City of Port Colborne.

The analysis has concluded that the proposed Rosedale Subdivision development will discharge a peak dry weather flow of approximately 8.55L/s and a peak wet weather flow of 11.87L/s to the downstream municipal sanitary sewer system. With the combination of the proposed development and surrounding properties, the existing downstream municipal sanitary sewer system reaches maximum capacities of approximately 75% upon reaching the Elm Street Dog Park south property limit. This includes numerous areas of currently undeveloped industrial lands within Drainage Areas E5, E6, E8 and E9. Therefore, it is expected that the downstream municipal sanitary infrastructure will have sufficient capacity for the proposed development.

Previous conversations occurred with the Niagara Region discussing the possibility of discharging sanitary flows from the existing Oxford Boulevard SPS into the proposed development to ultimately be included within the Industrial Park SPS Overall Drainage Area. As such, two additional calculation sheets have been included in Appendix B. The first calculation sheet includes an additional flow of 7.6L/s per the Oxford SPS ECA Firm Capacity which ultimately increases the downstream maximum sanitary sewer capacity to 93.2%. The second sanitary calculation sheet includes the sanitary flow rate calculated by UCC for the Oxford Boulevard SPS, concluding in a flow rate of 4.49L/s. This would result in a maximum downstream sanitary capacity of 85.7%. However, no further details have been provided by the Region on this matter, and as such, these additional flows are not expected to be included in the future Rosedale Subdivision sanitary sewer design.

STORMWATER MANAGEMENT PLAN

As part of the site development, the following is a summary of the stormwater management plan for the proposed residential development.

The criteria provided by the City of Port Colborne and Region of Niagara for this development includes the requirement to control peak stormwater flows from the proposed development area to



existing levels up to and including the 100 year design storm event and improve stormwater quality levels to MECP Normal (70% TSS removal) Protection levels prior to discharge from the development.

To limit future stormwater flows to allowable levels, and improve stormwater quality to the required TSS removal levels, a Stormwater Management (SWM) Wetpond Facility will provide the necessary controls for this development. The SWM facility will be located at the north limit of the proposed development and discharge stormwater flows to a storm sewer located at the north-west corner of the site. Stormwater flows will then be directed to the Biederman Drain north of the site. Stormwater quality levels will be treated to a Normal Standard (70% TSS removal) before discharging from the development site.

Stormwater flows up to and including the 5 year design storm event will be directed to the SWM facility via storm sewers. During major storm events greater than the 5 year event, stormwater flows unable to enter the storm sewer system will be directed overland towards to the SWM facility. Additionally, overland stormwater flows from the adjacent Meadow Heights Subdivision will be directed to the Rosedale Subdivision SWM Facility. A Stormwater Management Plan for this development has been created and can be found in Appendix C.



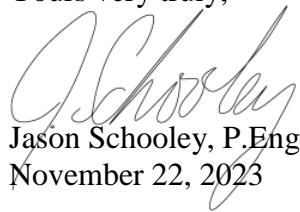
CONCLUSIONS AND RECOMMENDATIONS

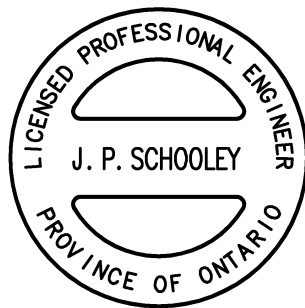
Therefore, based on the above comments and design calculations provided for this site, the following summarizes the servicing for this site.

1. The existing municipal watermain system will have sufficient capacity to provide both domestic and fire protection water supply.
2. The existing municipal sanitary sewer system downstream of the site will have adequate capacity for the proposed residential development.
3. Stormwater quality controls are being provided to Normal Protection (70% TSS removal) levels by a stormwater wetpond facility before outletting to the Biederman Drain.
4. Stormwater quantity controls are being provided by a stormwater management wetpond facility up to the 100 year design storm event prior to discharging from the site.
5. The site stormwater overland route from the road system is to the proposed stormwater management facility before outletting to the Biederman Drain.

Based on the above and the accompanying Stormwater Management Brief, there exists adequate municipal servicing for this development. We trust the above comments and enclosed calculations are satisfactory for approval. If you have any questions or require additional information, please do not hesitate to contact our office.

Yours very truly,


Jason Schooley, P.Eng.
November 22, 2023



Encl.



**UPPER CANADA
CONSULTANTS**
ENGINEERS / PLANNERS

APPENDICES



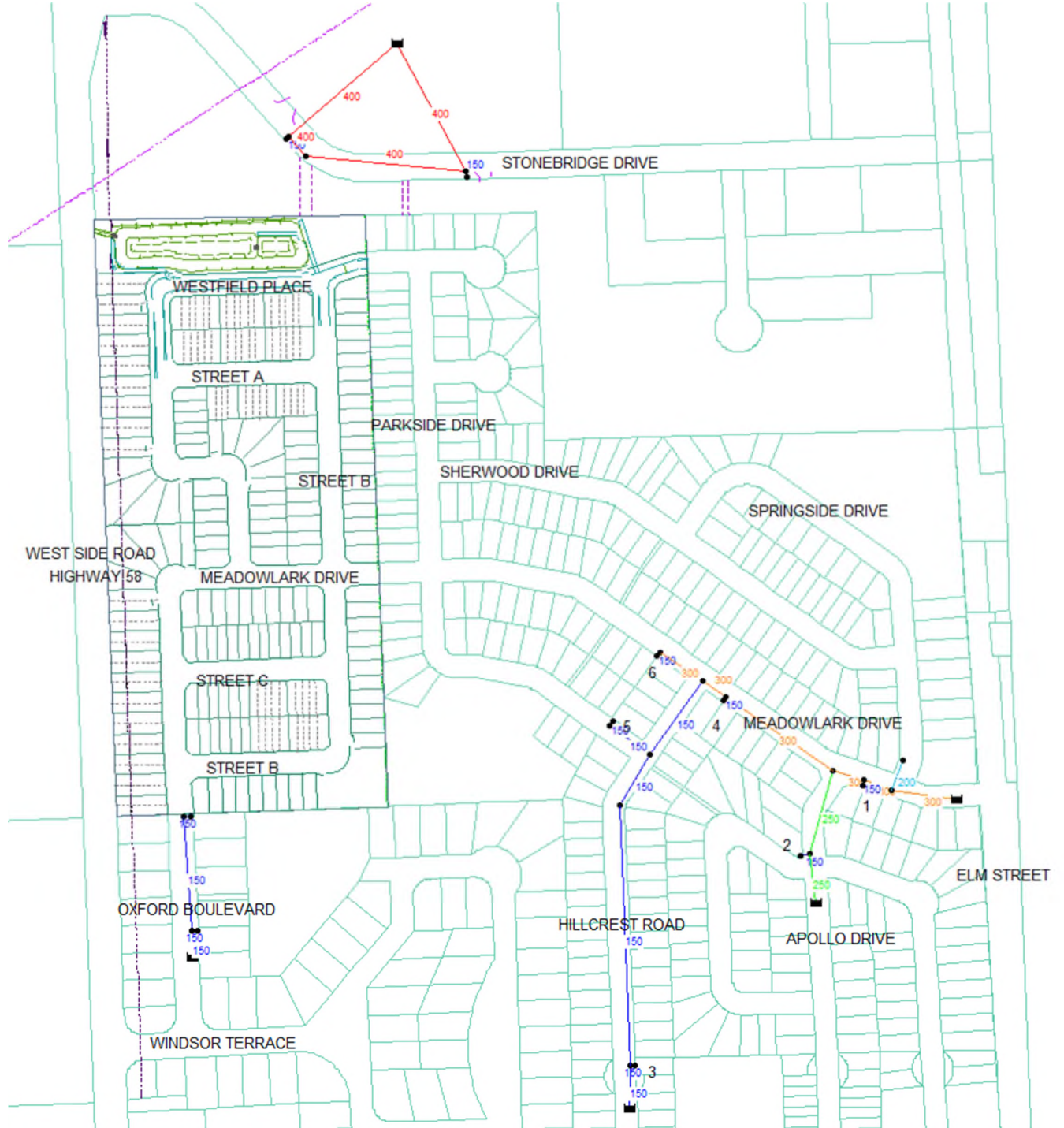
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APPENDIX A

EPANET – Existing Conditions Imagery (Sewer Diameters)
EPANET – Existing Conditions Imagery (Static Pressures in m of H₂O)
EPANET – Future Conditions Imagery (Sewer Diameters)
EPANET – Future Conditions Imagery (Static Pressures in m of H₂O)
EPANET Analysis Calculations
Rosedale Subdivision Preliminary Grading Design

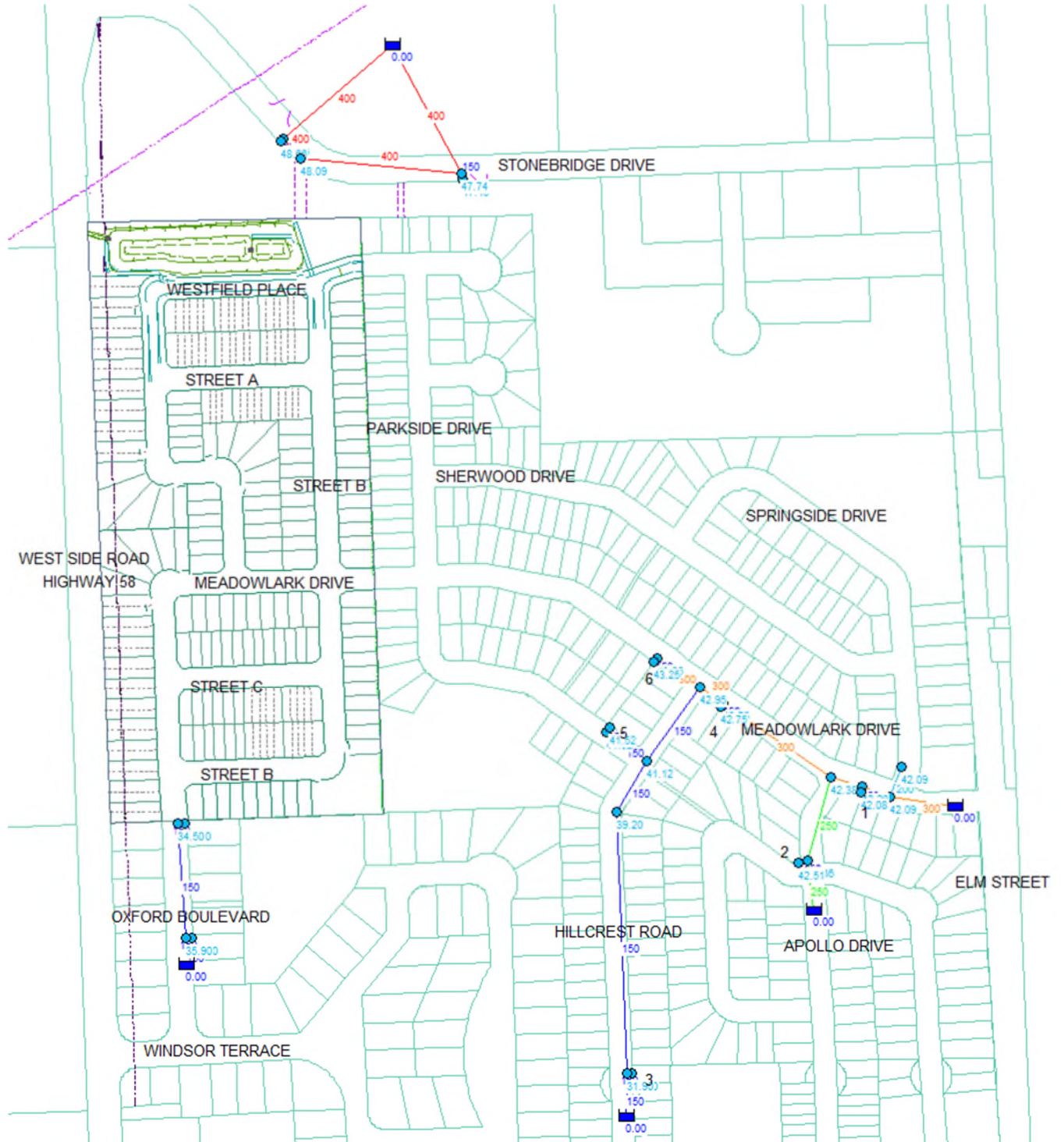


EPANET Imagery – Existing Conditions with Pipe Diameters (mm)



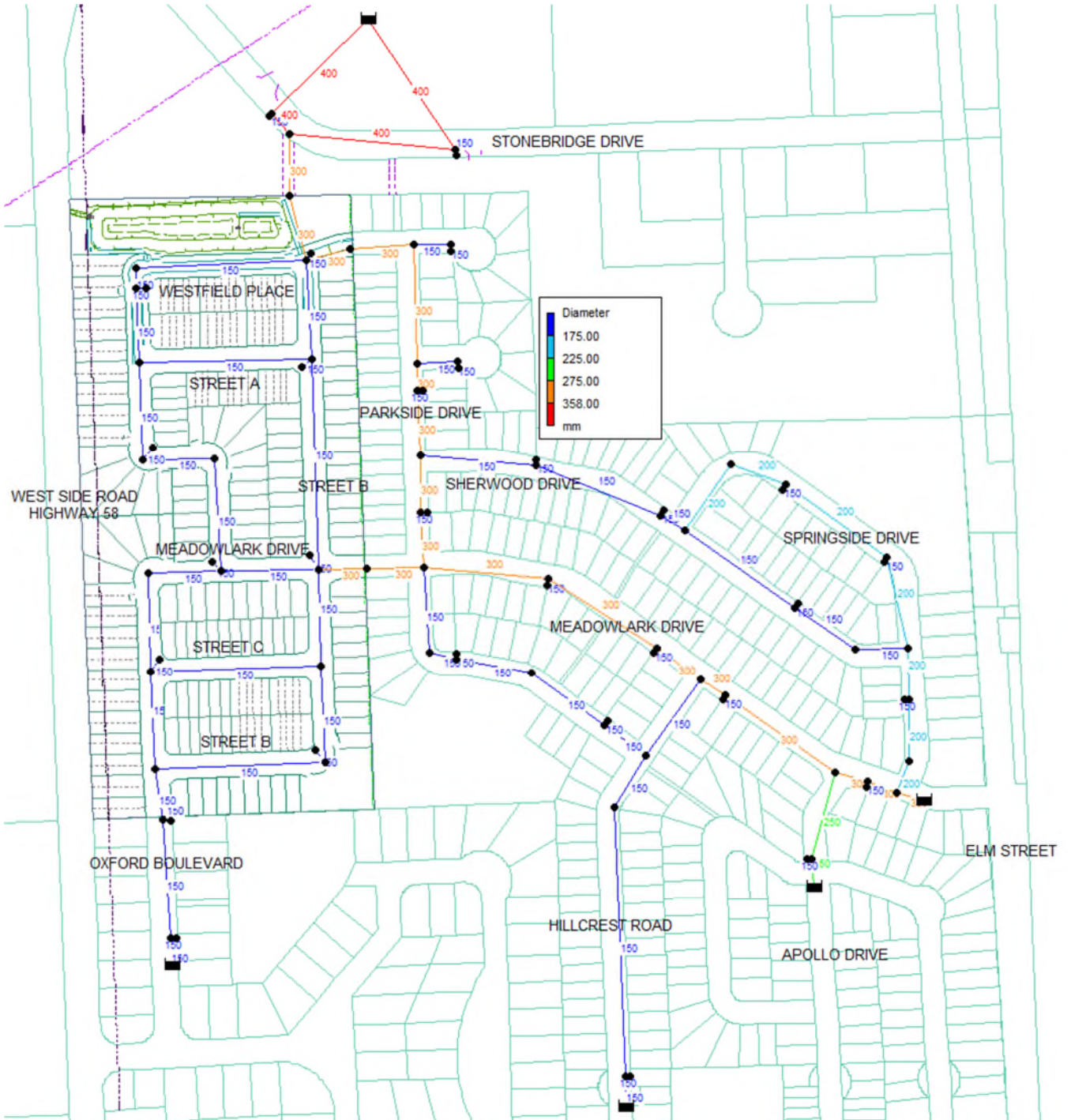


EPANET Imagery – Existing Conditions with Static Pressures (m of H₂O)



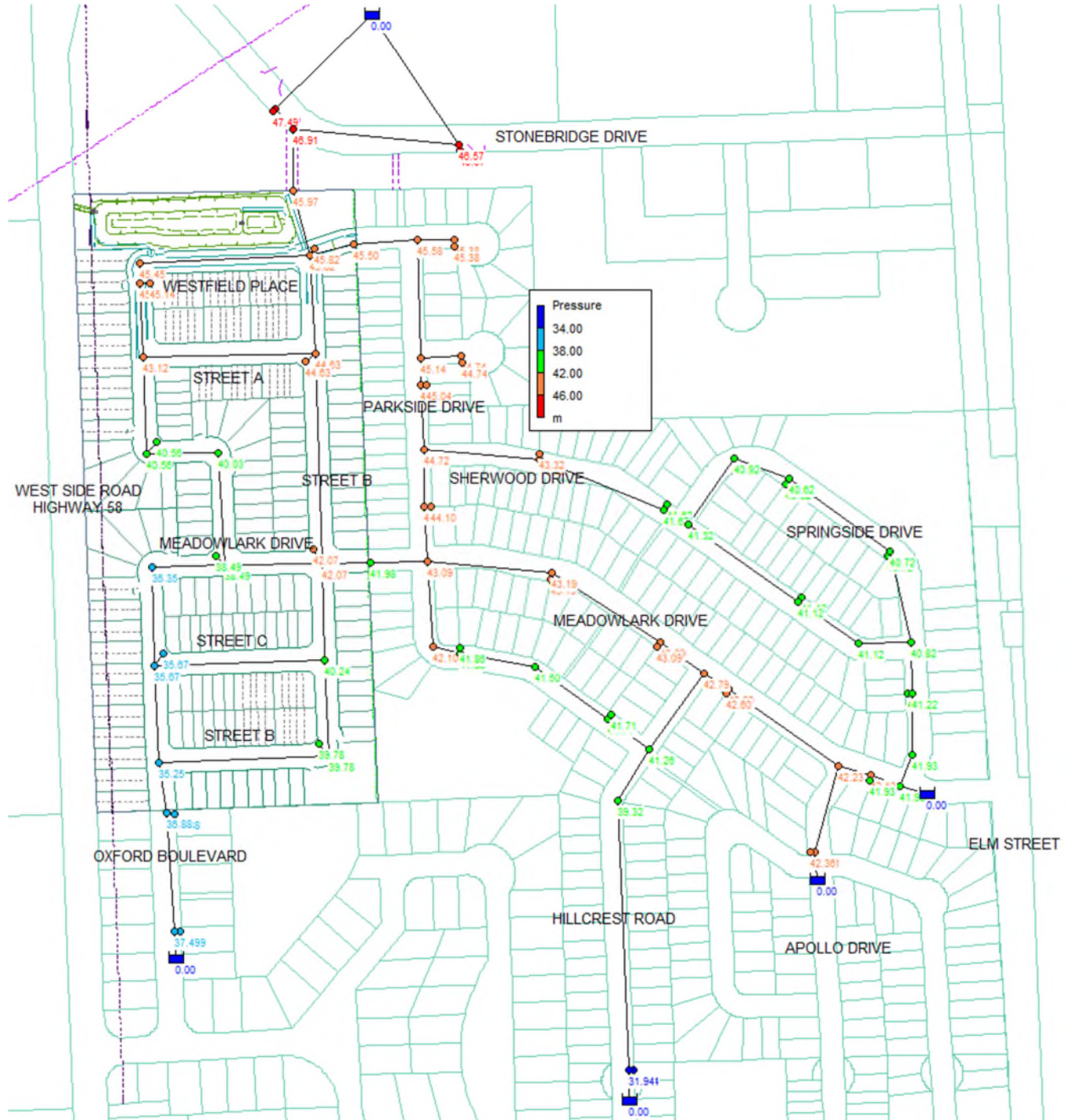


EPANET Imagery – Future Conditions with Pipe Diameters (mm)





EPANET Imagery – Future Conditions with Static Pressures (m of H2O)



ROSEDALE SUBDIVISION EPANET WATER MODEL CALCULATIONS

Hyd Number	Key Street	Hydrant Address	Hydrant Data		Existing Modelled		Future Modelled (with Rosedale)			Hydrant Data		Existing Modelled		Hydrant Data			Hydrant Data		Existing Modelled		Future Modelled with Rosedale	
			Static (PSI)	Static (m of H2O)	Static (m of H2O)	% Difference	Modelled Static Pressures (m of H2O)	Modelled Static Pressures (PSI)	% Difference	Residual PSI	Residual (m of H2O)	Modelled Residual	% Difference	Residual Hydrant No.	Actual Flow (GPM)	Actual Flow (LPS)	Theoretical Flow (GPM @ 20psi)	Theoretical Flow (LPS @ 20psi)	Modelled Theoretical Flow (LPS @ 14.06m)	% Difference	Fire Flow (LPS @ 14.06m)	Fire Flow GPM
63000009	APOLLO DRIVE	APOLLO DRIVE @ ORIOLE CRESCENT	62	43.6	42.5	-2.5%	42.4	60.3	-0.2%	52	36.6	35.2	3.7%	20	1350	85.2	2930	184.9	185	0.1%	293	4644
63000020	MEADOWLARK DRIVE	120M WEST OF ELM STREET	58	40.8	42.1	3.2%	41.9	59.6	-0.5%	50	35.2	35.3	-0.4%	9	1306	82.4	3030	191.2	186	-2.7%	311	4929
63000304	HILLCREST ROAD	IN FRONT OF # 59 HILLCREST ROAD	45	31.6	31.9	0.8%	31.9	45.4	0.0%	36	25.3	25.7	-1.5%	305	1216	76.7	2111	133.2	133	-0.1%	138	2187
63000157	OXFORD BOULEVARD	IN FRONT OF # 10 OXFORD BOULEVARD	50	35.2	35.9	2.1%	37.5	53.3	4.5%	41	28.8	29.3	-1.6%	156	631	39.8	1213	76.5	76	-0.7%	146	2314
63000158	OXFORD BOULEVARD	IN FRONT OF # 20 OXFORD BOULEVARD	50	35.2	34.5	-1.9%	36.9	52.5	7.0%	39	27.4	27.3	0.5%	157	533	33.6	916	57.8	59	2.1%	148	2346
63000160	STONEBRIDGE DRIVE	2ND HYD EAST OF HWY # 58 ON STONEBRIDGE DRIVE	70	49.2	48.7	-1.0%	47.5	67.6	-2.5%	57	40.1	38.2	4.7%	159	1686	106.4	3490	220.2	204	-7.4%	378	5991
63000283	STONEBRIDGE DRIVE	2ND W. OF PETERSBURG CIRCLE ON STONEBRIDGE DRIVE	67	47.1	47.5	0.8%	46.6	66.3	-1.9%	54	38.0	38.9	-2.4%	160	1508	95.1	3019	190.5	200	5.0%	365	5785

Conversions

PSI	m of H2O
1	0.703
20	14.062
40	28.124
50	35.154
80	56.247

Column Explanation

Column	Explanation
A	Static pressures in PSI provided by City
B	Static Pressures converted to m of H2O
C	Static Pressures (in m of H2O) from EPANET model attempting to replicate Column B values
D	% difference of Hydrant Data and Existing Model static pressures (Columns D & B)
E	New Modelled Pressures with inclusion of Rosedale and Meadow Heights Subdivisions
F	Pressures in Column E converted back to PSI
G	% difference of existing and future modelled static pressures (Columns C & E)
H	Residual Pressures in PSI provided by City
I	Residual Pressures converted to m of H2O
J	Residual Pressures (in m of H2O) from EPANET model attempting to replicate Column I values
K	% difference of Hydrant Data and Existing Model Residual Pressures (Columns Q & R)
L	Hydrant Number utilized to complete residual hydrant flow test
M	Actual Residual Flow data provided by City in GPM
N	Actual Residual Flow data provided by City converted to LPS
O	Theoretical Fire Flows in GPM at 20 PSI provided by City
P	Theoretical Fire Flows provided by City converted to LPS
Q	Theoretical Fire Flows in LPS (@ 14.06 m of H2O) from EPANET model attempting to replicate Column P values
R	% difference of city calculated existing theoretical flow and modelled theoretical flow at 20 PSI (Columns P & Q)
S	Calculated Fire Flows (@ 20PSI) calculated for future conditions with Rosedale Subdivision in LPS
T	Column S values converted to GPM
Average	320
Max Day	570
Peak	860

Node	Street	# of Houses	Population	Average Flow (LPS)	Max Day Flow (LPS)	Peak Day Flow (LPS)	Modelled Peak Day Hydrant Flow @ 20
1	Meadowlark	16	48	0.18	0.11	0.48	311
2	Apollo	12	36	0.13	0.24	0.36	293
3	Hillcrest	12	36	0.13	0.24	0.36	138
4	Meadowlark	11	33	0.12	0.22	0.33	
5	Parkside	7	21	0.08	0.14	0.21	183
6	Meadowlark	9	27	0.10	0.18	0.27	347
7	Springside	21	63	0.23	0.42	0.63	
8	Springside	19	57	0.21	0.38	0.57	193
9	Springside	22	66	0.24	0.44	0.66	184
10	Sherwood	21	63	0.23	0.42	0.63	155
11	Sherwood	19	57	0.21	0.38	0.57	179
12	Sherwood	17	51	0.19	0.34	0.51	
13	Meadowlark	18	54	0.20	0.36	0.54	
14	Parkside	14	42	0.16	0.28	0.42	179
15	Parkside	13	39	0.14	0.26	0.39	
16	Parkside	21	63	0.23	0.42	0.63	
17	Aintree	14	42	0.16	0.28	0.42	
18	Westfield	24	72	0.27	0.48	0.72	
19	Westfield	25	75	0.28	0.49	0.75	
20	Westfield	38	114	0.42	0.75	1.13	186
21	Westfield	35	105	0.39	0.69	1.05	155
22	Street B	40	120	0.44	0.79	1.19	
23	Meadowlark	28	84	0.31	0.55	0.84	
24	Meadowlark	28	84	0.31	0.55	0.84	201
25	Oxford	34	102	0.38	0.67	1.02	169
26	Street B	39	117	0.43	0.77	1.16	150
27	Oxford	23	69	0.26	0.46	0.69	148

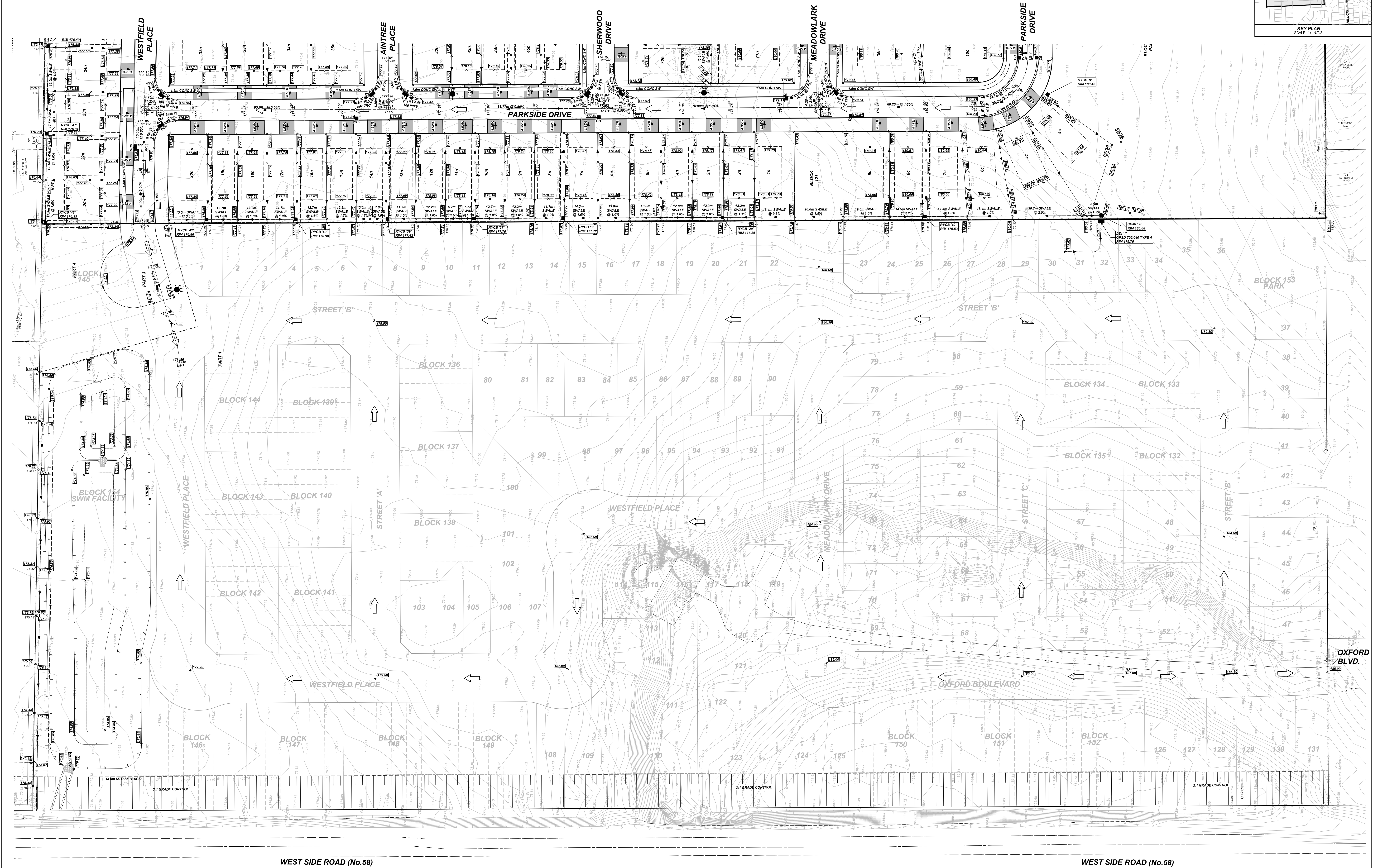
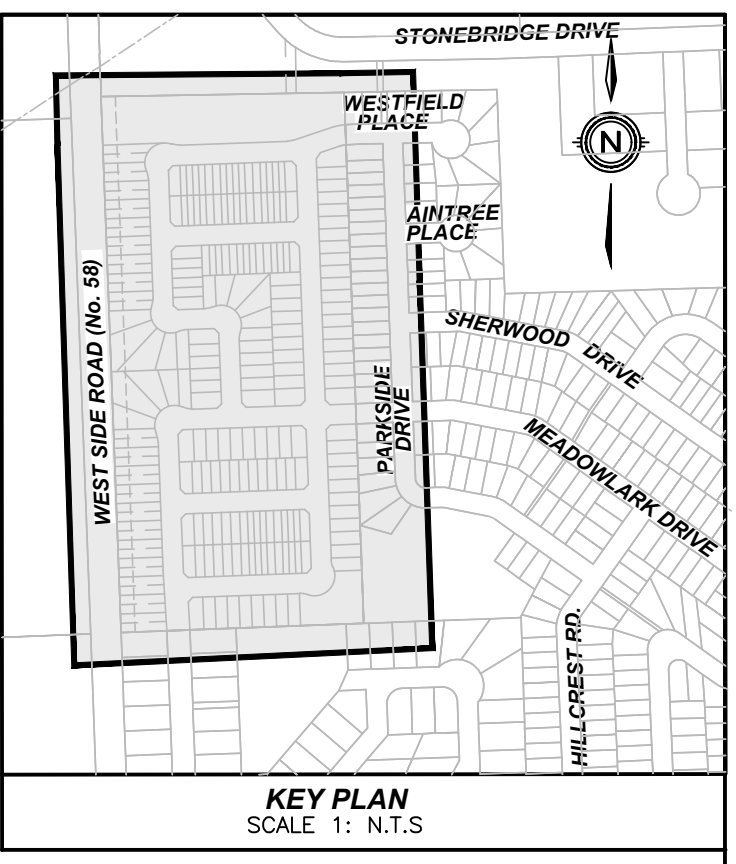
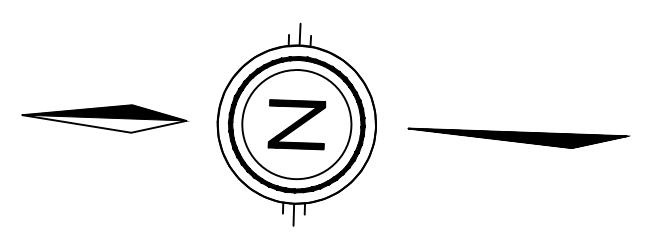
WORST CASE

WORST NEW CASE

WORST NEW CASE

Total Average 0.24 0.42 0.64
Rosedale Average 0.36 0.64 0.97

Rosedale
Average Day (0.36) use 0.40 everywhere
Max Day (0.64) use 0.70 everywhere
Peak Day (0.96) use 1.0 everywhere



WEST SIDE ROAD (No.58)

WEST SIDE ROAD (No.58)

NO.	REVISION	DATE	INIT
0	ISSUED FOR REVIEW	2023-10-16	BV
#	REVISION	DATE	INIT

NOTES:

1. THE POSITION OF POLE LINES, CONDUITS, WATERMANS, SEWER, AND OTHER UNDERGROUND AND OVERGROUND UTILITIES AND STRUCTURES IS NOT NECESSARILY SHOWN ON THE CONTRACT DRAWINGS AND, WHILE SHOWING THE ACCURACY OF THE POSITION OF SUCH UTILITIES AND STRUCTURES IS NOT GUARANTEED, BEFORE STARTING WORK, THE CONTRACTOR SHALL VERIFY THE LOCATION OF ALL SUCH UTILITIES AND STRUCTURES.
2. PROPERTY LINES WERE PLOTTED USING REGISTERED PLANS AND BARS LOCATED IN THE FIELD. TO VERIFY THE ACCURACY OF THESE PROPERTY LINES, A LEGAL SURVEY SHOULD BE PERFORMED PRIOR TO CONSTRUCTION.
3. ALL CONSTRUCTION MUST COMPLY WITH THE HANNA PROVINCE STANDARD CONTRACT DOCUMENT.

DRAFTING	BV
DESIGN	MH
CHECKED BY	MH
APPROVED BY	AK



OWNER
1399908 ONTARIO LTD
 O/A MEADOW HEIGHTS
 1510-105 MAIN STREET EAST
 HAMILTON, ON
 L8N 1G6

MEADOW HEIGHTS- PHASE 3
ROSEDALE PRELLIMINARY GRADING DESIGN
 CITY OF PORT COLBORNE

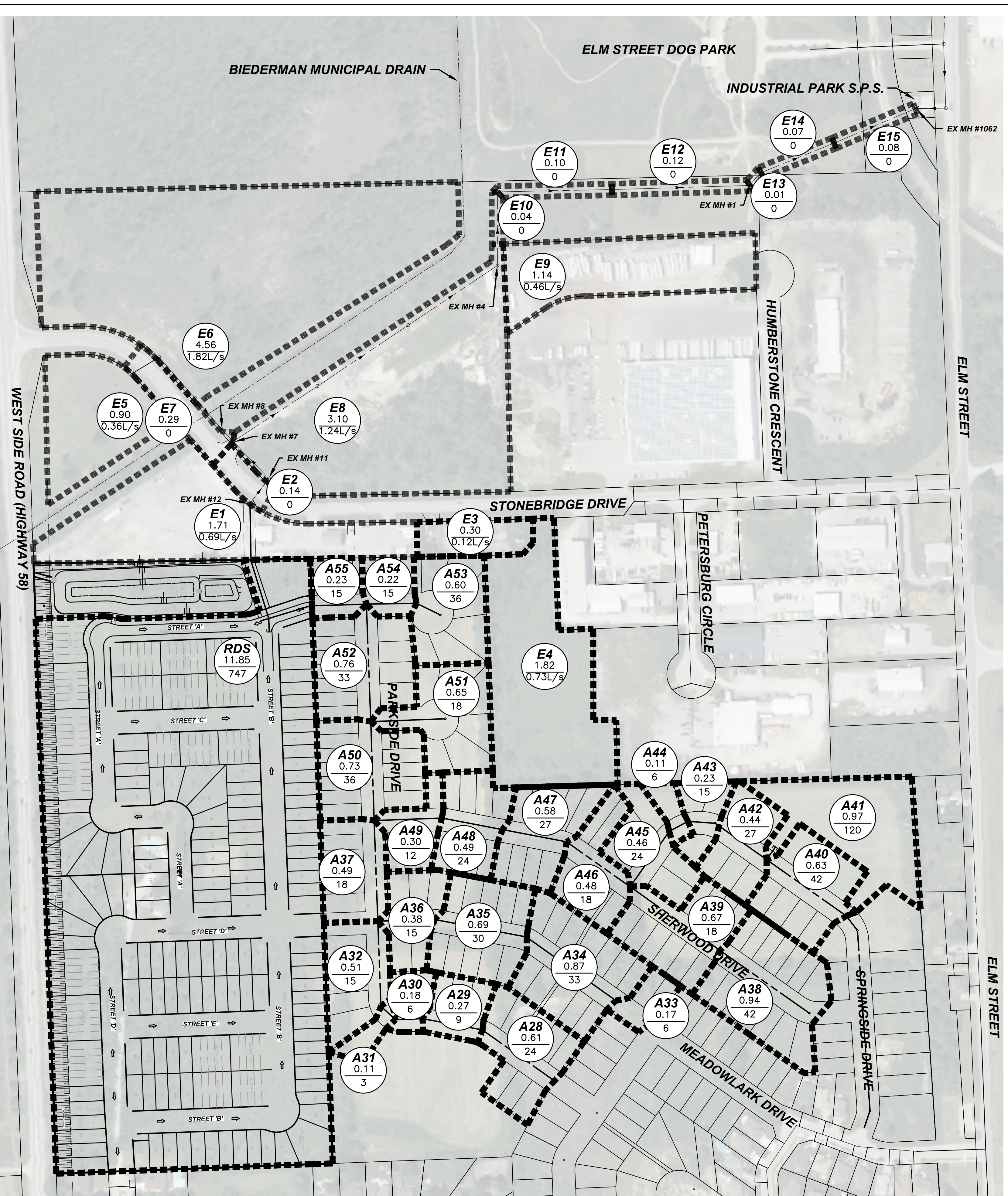
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REV	0



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APPENDIX B

Overall Sanitary Drainage Area Plan – Proposed Conditions
Overall Sanitary Calculations – with Regional MSP Oxford SPS Flows
Overall Sanitary Calculations – with UCC Oxford SPS Flows



UPPER CANADA CONSULTANTS
3-30 HANNOVER DRIVE
ST. CATHARINES, ONTARIO
L2W 1A5

DESIGN FLOWS
RESIDENTIAL: 255 LITRES/PERSON/DAY (AVERAGE DAILY FLOW)
INDUSTRIAL: 0.2 LITRES/SECOND GROSS HECTARE (MECP ALLOWANCE IS 0.2 - 0.64)
INFILTRATION RATE: 0.28 L/s/ha (M.O.E FLOW ALLOWANCE IS BETWEEN 0.10 & 0.28 L/s/ha)
POPULATION DENSITY: 3.0 PERSONS/UNIT

MUNICIPALITY: CITY OF PORT COLBORNE
PROJECT: MEADOW HEIGHTS
PROJECT NO: 227

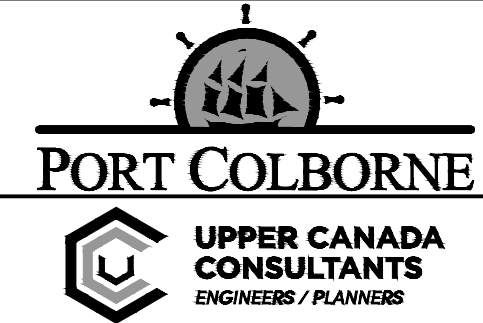
SEWER DESIGN
PIPE ROUGHNESS: 0.013 FOR MANNING'S EQUATION
PIPE SIZES: 1.016 IMPERIAL EQUIVALENT FACTOR
PERCENT FULL: TOTAL PEAK FLOW / CAPACITY

OVERALL SANITARY SEWER DESIGN SHEET
Peaking Factor = $M = 1 + \frac{14}{4 + \sqrt{P}}$ Where P = design population in thousands

Location and Description	From M.H.	To M.H.	AREA		POPULATION			ACCUMULATED PEAK FLOW			DESIGN FLOW					Percent Full		
			Increment (hectares)	Accumulated (hectares)	Number of Units	Population Density (persons/unit)	Population Increment	Total Population Served	Peaking Factor	Flow (L/s)	Infiltration Flow (L/s)	Total Peak Flow (L/s)	Pipe Diameter (mm)	Pipe Length (m)	Pipe Slope (%)		Full Flow Velocity (m/s)	Full Flow Capacity (L/s)
A28 - PARKSIDE DRIVE			0.61	0.61	8	3.0	24	24	4.37	0.31	0.17	0.48	200	60.0	0.40	0.67	21.64	2.2%
A29 - PARKSIDE DRIVE			0.27	0.88	3	3.0	9	33	4.35	0.42	0.25	0.67	200	52.9	0.40	0.67	21.64	3.1%
A30 - PARKSIDE DRIVE			0.18	1.06	2	3.0	6	39	4.34	0.50	0.30	0.80	200	23.7	0.40	0.67	21.64	3.7%
A31 - PARKSIDE DRIVE			0.11	1.17	1	3.0	3	42	4.33	0.54	0.33	0.86	200	17.2	0.40	0.67	21.64	4.0%
A32 - PARKSIDE DRIVE			0.52	1.69	5	3.0	15	57	4.30	0.72	0.47	1.20	200	74.1	1.50	1.29	41.91	2.9%
A33 - MEADOWLARK DRIVE			0.17	0.17	2	3.0	6	6	4.43	0.08	0.05	0.13	200	29.7	0.80	0.94	30.60	0.4%
A34 - MEADOWLARK DRIVE			0.87	1.04	11	3.0	33	39	4.34	0.50	0.29	0.79	200	95.6	0.40	0.67	21.64	3.7%
A35 - MEADOWLARK DRIVE			0.69	1.73	10	3.0	30	69	4.28	0.87	0.48	1.36	200	81.7	0.40	0.67	21.64	6.3%
A36 - MEADOWLARK DRIVE			0.38	2.11	5	3.0	15	84	4.26	1.06	0.59	1.65	200	49.3	0.40	0.67	21.64	7.6%
A37 - PARKSIDE DRIVE			0.49	4.29	6	3.0	18	159	4.18	1.96	1.20	3.16	200	87.8	0.87	0.98	31.92	9.9%
A38 - SHERWOOD DRIVE			0.94	0.94	14	3.0	42	42	4.33	0.54	0.26	0.80	200	95.0	0.80	0.94	30.60	2.6%
A39 - SHERWOOD DRIVE			0.67	1.61	10	3.0	30	72	4.28	0.91	0.45	1.36	200	96.0	0.40	0.67	21.64	6.3%
A40 - SPRINGSIDE DRIVE			0.63	0.63	14	3.0	42	42	4.33	0.54	0.18	0.71	200	70.6	0.40	0.67	21.64	3.3%
A41 - CONDO			0.97	0.97	40	3.0	120	120	4.22	1.49	0.27	1.77	200	13.6	0.40	0.67	21.64	8.2%
A42 - SPRINGSIDE DRIVE			0.44	2.04	9	3.0	27	189	4.16	2.32	0.57	2.89	200	54.9	0.40	0.67	21.64	13.4%
A43 - SPRINGSIDE DRIVE			0.23	2.27	5	3.0	15	204	4.14	2.50	0.64	3.13	200	23.8	0.50	0.75	24.19	12.9%
A44 - SPRINGSIDE DRIVE			0.11	2.38	2	3.0	6	210	4.14	2.57	0.67	3.23	200	18.5	0.40	0.67	21.64	14.9%
A45 - SPRINGSIDE DRIVE			0.46	2.84	8	3.0	24	234	4.12	2.85	0.80	3.64	200	59.1	0.40	0.67	21.64	16.8%
A46 - SHERWOOD DRIVE			0.48	4.93	6	3.0	18	324	4.06	3.89	1.38	5.27	200	67.7	0.92	1.01	32.82	16.0%
A47 - SHERWOOD DRIVE			0.58	5.51	9	3.0	27	351	4.05	4.19	1.54	5.74	200	56.9	0.88	0.99	32.10	17.9%
A48 - SHERWOOD DRIVE			0.49	6.00	8	3.0	24	375	4.04	4.47	1.68	6.15	200	53.7	1.35	1.23	39.76	15.5%
A49 - SHERWOOD DRIVE			0.30	6.30	4	3.0	12	387	4.03	4.60	1.76	6.37	200	59.1	1.35	1.23	39.76	16.0%
A50 - PARKSIDE DRIVE			0.73	11.32	12	3.0	36	582	3.94	6.77	3.17	9.94	200	86.3	0.40	0.67	21.64	45.9%
A51 - Aintree Place			0.65	0.65	12	3.0	36	36	4.34	0.46	0.18	0.64	200	65.0	1.00	1.06	34.22	1.9%
A52 - PARKSIDE DRIVE			0.76	12.73	15	3.0	45	663	3.91	7.65	3.56	11.21	200	102.5	0.40	0.67	21.64	51.8%
A53 - WESTFIELD PLACE			0.60	0.60	12	3.0	36	36	4.34	0.46	0.17	0.63	200	23.1	1.00	1.06	34.22	1.8%
A54 - WESTFIELD PLACE			0.22	0.82	5	3.0	15	51	4.31	0.65	0.23	0.88	200	43.7	0.40	0.67	21.64	4.1%
A55 - WESTFIELD PLACE			0.23	13.78	5	3.0	15	729	3.88	8.36	3.86	12.22	200	49.2	0.40	0.67	21.64	56.4%
WESTFIELD PLACE				13.78				729	3.88	8.36	3.86	12.22	200	37.6	0.40	0.67	21.64	56.4%
RDS - ROSEDALE			11.85		249	3.0	747	747	3.88	8.55	3.32	11.87						
EASEMENT - ROSEDALE				25.63				1476	3.68	16.05	7.18	23.23	300	52.4	0.37	0.84	61.36	37.9%
EASEMENT - VAN JON		EXMH 12		25.63				1476	3.68	16.05	7.18	23.23	300	48.8	0.43	0.91	66.15	35.1%
E1 - VAN JON PAVING			1.72					2.00	0.69									
E2 - STONEBRIDGE DR	EXMH 12	EXMH 11	0.14	27.49				1476	3.68	16.05	7.70	24.44	300	28.0	0.29	0.74	54.33	45.0%
E3 - INDUSTRIAL LANDS			0.30					2.00	0.12									
E4 - INDUSTRIAL LANDS			1.82					2.00	0.73									
STONEBRIDGE DR	EXMH 11	EXMH 7		27.49				1476	3.68	16.05	7.70	24.44	300	45.0	0.20	0.62	45.12	54.2%
E5 - INDUSTRIAL LANDS			0.90					2.00	0.36									
E6 - INDUSTRIAL LANDS			4.56					2.00	1.82									
E7 - STONEBRIDGE DR	EXMH 8	EXMH 7	0.29	5.75				2.00	1.24	1.61	3.79	300	16.0	1.09	1.44	105.32	3.6%	
E8 - INDUSTRIAL LANDS	EXMH 7	EXMH 6	3.10	3.10				2.00	0.12									
INDUSTRIAL LANDS	EXMH 7	EXMH 6		36.34				1476	3.68	16.05	10.18	30.34	300	88.8	0.20	0.62	45.12	67.2%
INDUSTRIAL LANDS	EXMH 6	EXMH 5		36.34				1476	3.68	16.05	10.18	30.34	300	94.8	0.20	0.62	45.12	67.2%
INDUSTRIAL LANDS	EXMH 5	EXMH 4		36.34				1476	3.68	16.05	10.18	30.34	300	92.6	0.24	0.68	49.42	61.4%
INDUSTRIAL LANDS	EXMH 4	EXMH 3	1.14					2.00	0.46									
E10 - INDUSTRIAL LANDS	EXMH 4	EXMH 3	0.04	37.52				1476	3.68	16.05	10.51	31.12	300	64.7	0.27	0.72	52.42	59.4%
ELM ST DOG PARK	EXMH 3	EXMH 2	0.10	37.62				1476	3.68	16.05	10.53	31.15	300	99.8	0.17	0.57	41.59	74.9%
ELM ST DOG PARK	EXMH 2	EXMH 1	0.12	37.74				1476	3.68	16.05	10.57	31.19	300	120.4	0.21	0.63	46.23	67.5%
ELM ST DOG PARK	EXMH 1	EX 1042	0.01	37.75				1476	3.68	16.05	10.57	31.19	300	14.0	0.22	0.65	47.32	65.9%
ELM ST DOG PARK	EX 1042	EX 1043	0.07	37.82				1476	3.68	16.05	10.59	31.21	300	69.0	0.22	0.65	47.32	66.0%
ELM ST DOG PARK	EX 1043	EX 1062	0.08	37.90				1476	3.68	16.05	10.61	31.23	300	77.0	0.22	0.65	47.32	66.0%

NOTES:
1. THE POSITION OF POLE LINES, CONDUITS, WATERMANS, SEWER, AND OTHER UNDERGROUND AND OVERGROUND UTILITIES AND STRUCTURES IS NOT NECESSARILY SHOWN ON THE CONTRACT DRAWINGS AND, WHERE SHOWN, THE ACCURACY OF THE POSITION OF SUCH UTILITIES AND STRUCTURES IS NOT GUARANTEED. BEFORE STARTING WORK, THE CONTRACTOR SHALL INFORM HIMSELF OF THE EXACT LOCATION OF ALL SUCH UTILITIES AND STRUCTURES AND SHALL ASSUME ALL LIABILITY FOR DAMAGE TO THEM.
2. PROPERTY LINES WERE PLOTTED USING REGISTERED PLANS AND BARS LOCATED IN THE FIELD. TO VERIFY THE ACCURACY OF THESE PROPERTY LINES, A LEGAL SURVEY SHOULD BE PERFORMED PRIOR TO CONSTRUCTION.
3. ALL CONSTRUCTION MUST COMPLY WITH THE NIAGARA PENINSULA STANDARD CONTRACT DOCUMENT.

DRAFTING	KT
DESIGN	KT
CHECKED BY	JS
APPROVED BY	JS



ROSEDALE / MEADOW HEIGHTS
CITY OF PORT COLBORNE
OVERALL SANITARY DRAINAGE AREA PLAN

CONSULTANT FILE No.	###
DATE	2023-11-22
PRINTED	2023-11-22
SCALE	1:500 m
REF No.	
DWG No.	###
REV	0

UPPER CANADA CONSULTANTS

3-30 HANNOVER DRIVE
ST.CATHARINES, ONTARIO
L2W 1A3

INCLUDING OXFORD BOULEVARD SANITARY SEWER FLOWS PER REGIONAL MSP UPDATE

DESIGN FLOWS

RESIDENTIAL: 255 LITRES/PERSON/DAY (AVERAGE DAILY FLOW)
INDUSTRIAL: 0.2 LITRES/SECOND/GROSS HECTARE (MECP ALLOWANCE IS 0.2 - 0.64)
INFILTRATION RATE: 0.28 L / s / ha (M.O.E FLOW ALLOWANCE IS BETWEEN 0.10 & 0.28 L / s / ha)
POPULATION DENSITY: 3.0 PERSONS / UNIT

SEWER DESIGN

PIPE ROUGHNESS: 0.013 FOR MANNING'S EQUATION
PIPE SIZES: 1.016 IMPERIAL EQUIVALENT FACTOR
PERCENT FULL: TOTAL PEAK FLOW / CAPACITY

MUNICIPALITY: CITY OF PORT COLBORNE

PROJECT : MEADOW HEIGHTS

PROJECT NO: 227

OVERALL SANITARY SEWER DESIGN SHEET

Peaking Factor= $M = 1 + \frac{14}{4 + P^{0.5}}$ Where P = design population in thousands

LOCATION			AREA		POPULATION				ACCUMULATED PEAK FLOW				DESIGN FLOW					Percent Full
Location and Description	From M.H	To M.H.	Increment (hectares)	Accumulated (hectares)	Number of Units	Population Density (persons/unit)	Population Increment	Total Population Served	Peaking Factor	Flow (L/s)	Infiltration Flow L/s	Total Peak Flow (L/s)	Pipe Diameter (mm)	Pipe Length (m)	Pipe Slope (%)	Full Flow Velocity (m/s)	Full Flow Capacity (L/s)	
A28 - PARKSIDE DRIVE			0.61	0.61	8	3.0	24	24	4.37	0.31	0.17	0.48	200	60.0	0.40	0.67	21.64	2.2%
A29 - PARKSIDE DRIVE			0.27	0.88	3	3.0	9	33	4.35	0.42	0.25	0.67	200	52.9	0.40	0.67	21.64	3.1%
A30 - PARKSIDE DRIVE			0.18	1.06	2	3.0	6	39	4.34	0.50	0.30	0.80	200	23.7	0.40	0.67	21.64	3.7%
A31 - PARKSIDE DRIVE			0.11	1.17	1	3.0	3	42	4.33	0.54	0.33	0.86	200	17.2	0.40	0.67	21.64	4.0%
A32 - PARKSIDE DRIVE			0.52	1.69	5	3.0	15	57	4.30	0.72	0.47	1.20	200	74.1	1.50	1.29	41.91	2.9%
A33 - MEADOWLARK DRIVE			0.17	0.17	2	3.0	6	6	4.43	0.08	0.05	0.13	200	29.7	0.80	0.94	30.60	0.4%
A34 - MEADOWLARK DRIVE			0.87	1.04	11	3.0	33	39	4.34	0.50	0.29	0.79	200	95.6	0.40	0.67	21.64	3.7%
A35 - MEADOWLARK DRIVE			0.69	1.73	10	3.0	30	69	4.28	0.87	0.48	1.36	200	81.7	0.40	0.67	21.64	6.3%
A36 - MEADOWLARK DRIVE			0.38	2.11	5	3.0	15	84	4.26	1.06	0.59	1.65	200	49.3	0.40	0.67	21.64	7.6%
A37 - PARKSIDE DRIVE			0.49	4.29	6	3.0	18	159	4.18	1.96	1.20	3.16	200	87.8	0.87	0.98	31.92	9.9%
A38 - SHERWOOD DRIVE			0.94	0.94	14	3.0	42	42	4.33	0.54	0.26	0.80	200	95.0	0.80	0.94	30.60	2.6%
A39 - SHERWOOD DRIVE			0.67	1.61	10	3.0	30	72	4.28	0.91	0.45	1.36	200	96.0	0.40	0.67	21.64	6.3%
A40 - SPRINGSIDE DRIVE			0.63	0.63	14	3.0	42	42	4.33	0.54	0.18	0.71	200	70.6	0.40	0.67	21.64	3.3%
A41 - CONDO			0.97	0.97	40	3.0	120	120	4.22	1.49	0.27	1.77	200	13.6	0.40	0.67	21.64	8.2%
A42 - SPRINGSIDE DRIVE			0.44	2.04	9	3.0	27	189	4.16	2.32	0.57	2.89	200	54.9	0.40	0.67	21.64	13.4%
A43 - SPRINGSIDE DRIVE			0.23	2.27	5	3.0	15	204	4.14	2.50	0.64	3.13	200	23.8	0.50	0.75	24.19	12.9%
A44 - SPRINGSIDE DRIVE			0.11	2.38	2	3.0	6	210	4.14	2.57	0.67	3.23	200	18.5	0.40	0.67	21.64	14.9%
A45 - SPRINGSIDE DRIVE			0.46	2.84	8	3.0	24	234	4.12	2.85	0.80	3.64	200	59.1	0.40	0.67	21.64	16.8%
A46 - SHERWOOD DRIVE			0.48	4.93	6	3.0	18	324	4.06	3.89	1.38	5.27	200	67.7	0.92	1.01	32.82	16.0%
A47 - SHERWOOD DRIVE			0.58	5.51	9	3.0	27	351	4.05	4.19	1.54	5.74	200	56.9	0.88	0.99	32.10	17.9%
A48 - SHERWOOD DRIVE			0.49	6.00	8	3.0	24	375	4.04	4.47	1.68	6.15	200	53.7	1.35	1.23	39.76	15.5%
A49 - SHERWOOD DRIVE			0.30	6.30	4	3.0	12	387	4.03	4.60	1.76	6.37	200	59.1	1.35	1.23	39.76	16.0%
A50 - PARKSIDE DRIVE			0.73	11.32	12	3.0	36	582	3.94	6.77	3.17	9.94	200	86.3	0.40	0.67	21.64	45.9%
A51 - AINTREE PLACE			0.65	0.65	12	3.0	36	36	4.34	0.46	0.18	0.64	200	65.0	1.00	1.06	34.22	1.9%
A52 - PARKSIDE DRIVE			0.76	12.73	15	3.0	45	663	3.91	7.65	3.56	11.21	200	102.5	0.40	0.67	21.64	51.8%
A53 - WESTFIELD PLACE			0.60	0.60	12	3.0	36	36	4.34	0.46	0.17	0.63	200	23.1	1.00	1.06	34.22	1.8%
A54 - WESTFIELD PLACE			0.22	0.82	5	3.0	15	51	4.31	0.65	0.23	0.88	200	43.7	0.40	0.67	21.64	4.1%
A55 - WESTFIELD PLACE			0.23	13.78	5	3.0	15	729	3.88	8.36	3.86	12.22	200	49.2	0.40	0.67	21.64	56.4%
WESTFIELD PLACE				13.78				729	3.88	8.36	3.86	12.22	200	37.6	0.40	0.67	21.64	56.4%
RDS - ROSEDALE			11.85		249	3.0	747	747	3.88	8.55	3.32	11.87						
OXFORD SPS (Per Regional MSP Update)			12.50				2051 Projected Population & Employment	453				7.60	ECA Firm Capacity per 2021 Regional MSP Update					
EASEMENT - ROSEDALE				25.63				1476	3.68	16.05	7.18	30.83	300	52.4	0.37	0.84	61.36	50.2%
EASEMENT - VAN JON		EXMH 12		25.63				1476	3.68	16.05	7.18	30.83	300	48.8	0.43	0.91	66.15	46.6%
E1 - VAN JON PAVING			1.72						2.00	0.69								
E2 - STONEBRIDGE DR	EXMH 12	EXMH 11	0.14	27.49				1476	3.68	16.05	7.70	32.04	300	28.0	0.29	0.74	54.33	59.0%
E3 - INDUSTRIAL LANDS			0.30						2.00	0.12								
E4 - INDUSTRIAL LANDS			1.82						2.00	0.73								
STONEBRIDGE DR	EXMH 11	EXMH 7		27.49				1476	3.68	16.05	7.70	32.04	300	45.0	0.20	0.62	45.12	71.0%
E5 - INDUSTRIAL LANDS			0.90						2.00	0.36								
E6 - INDUSTRIAL LANDS			4.56						2.00	1.82								
E7 - STONEBRIDGE DR	EXMH 8	EXMH 7	0.29	5.75							1.61	3.79	300	16.0	1.09	1.44	105.32	3.6%
E8 - INDUSTRIAL LANDS		EXMH 7	3.10	3.10					2.00	1.24								
INDUSTRIAL LANDS	EXMH 7	EXMH 6		36.34				1476	3.68	16.05	10.18	37.94	300	88.8	0.20	0.62	45.12	84.1%
INDUSTRIAL LANDS	EXMH 6	EXMH 5		36.34				1476	3.68	16.05	10.18	37.94	300	94.8	0.20	0.62	45.12	84.1%
INDUSTRIAL LANDS	EXMH 5	EXMH 4		36.34				1476	3.68	16.05	10.18	37.94	300	92.6	0.24	0.68	49.42	76.8%
E9 - INDUSTRIAL LANDS		EXMH 4	1.14						2.00	0.46								
E10 - INDUSTRIAL LANDS	EXMH 4	EXMH 3	0.04	37.52				1476	3.68	16.05	10.51	38.72	300	64.7	0.27	0.72	52.42	73.9%
ELM ST DOG PARK	EXMH 3	EXMH 2	0.10	37.62				1476	3.68	16.05	10.53	38.75	300	99.8	0.17	0.57	41.59	93.2%
ELM ST DOG PARK	EXMH 2	EXMH 1	0.12	37.74				1476	3.68	16.05	10.57	38.79	300	120.4	0.21	0.63	46.23	83.9%
ELM ST DOG PARK	EXMH 1	EX 1042	0.01	37.75				1476	3.68	16.05	10.57	38.79	300	14.0	0.22	0.65	47.32	82.0%
ELM ST DOG PARK	EX 1042	EX 1043	0.07	37.82				1476	3.68	16.05	10.59	38.81	300	69.0	0.22	0.65	47.32	82.0%
ELM ST DOG PARK	EX 1043	EX 1062	0.08	37.90				1476	3.68	16.05	10.61	38.83	300	77.0	0.22	0.65	47.32	82.1%

UPPER CANADA CONSULTANTS

3-30 HANNOVER DRIVE
ST.CATHARINES, ONTARIO
L2W 1A3

INCLUDING OXFORD BOULEVARD SANITARY SEWER FLOWS PER UCC CALCULATIONS

DESIGN FLOWS

RESIDENTIAL: 255 LITRES/PERSON/DAY (AVERAGE DAILY FLOW)
INDUSTRIAL: 0.2 LITRES/SECOND/GROSS HECTARE (MECP ALLOWANCE IS 0.2 - 0.64)
INFILTRATION RATE: 0.28 L / s / ha (M.O.E FLOW ALLOWANCE IS BETWEEN 0.10 & 0.28 L / s / ha)
POPULATION DENSITY: 3.0 PERSONS / UNIT

SEWER DESIGN

PIPE ROUGHNESS: 0.013 FOR MANNING'S EQUATION
PIPE SIZES: 1.016 IMPERIAL EQUIVALENT FACTOR
PERCENT FULL: TOTAL PEAK FLOW / CAPACITY

MUNICIPALITY: CITY OF PORT COLBORNE

PROJECT : MEADOW HEIGHTS

PROJECT NO: 227

OVERALL SANITARY SEWER DESIGN SHEET

Peaking Factor= $M = 1 + \frac{14}{4 + P^{0.5}}$ Where P = design population in thousands

LOCATION			AREA		POPULATION				ACCUMULATED PEAK FLOW				DESIGN FLOW					Percent Full
Location and Description	From M.H	To M.H.	Increment (hectares)	Accumulated (hectares)	Number of Units	Population Density (persons/unit)	Population Increment	Total Population Served	Peaking Factor	Flow (L/s)	Infiltration Flow L/s	Total Peak Flow (L/s)	Pipe Diameter (mm)	Pipe Length (m)	Pipe Slope (%)	Full Flow Velocity (m/s)	Full Flow Capacity (L/s)	
A28 - PARKSIDE DRIVE			0.61	0.61	8	3.0	24	24	4.37	0.31	0.17	0.48	200	60.0	0.40	0.67	21.64	2.2%
A29 - PARKSIDE DRIVE			0.27	0.88	3	3.0	9	33	4.35	0.42	0.25	0.67	200	52.9	0.40	0.67	21.64	3.1%
A30 - PARKSIDE DRIVE			0.18	1.06	2	3.0	6	39	4.34	0.50	0.30	0.80	200	23.7	0.40	0.67	21.64	3.7%
A31 - PARKSIDE DRIVE			0.11	1.17	1	3.0	3	42	4.33	0.54	0.33	0.86	200	17.2	0.40	0.67	21.64	4.0%
A32 - PARKSIDE DRIVE			0.52	1.69	5	3.0	15	57	4.30	0.72	0.47	1.20	200	74.1	1.50	1.29	41.91	2.9%
A33 - MEADOWLARK DRIVE			0.17	0.17	2	3.0	6	6	4.43	0.08	0.05	0.13	200	29.7	0.80	0.94	30.60	0.4%
A34 - MEADOWLARK DRIVE			0.87	1.04	11	3.0	33	39	4.34	0.50	0.29	0.79	200	95.6	0.40	0.67	21.64	3.7%
A35 - MEADOWLARK DRIVE			0.69	1.73	10	3.0	30	69	4.28	0.87	0.48	1.36	200	81.7	0.40	0.67	21.64	6.3%
A36 - MEADOWLARK DRIVE			0.38	2.11	5	3.0	15	84	4.26	1.06	0.59	1.65	200	49.3	0.40	0.67	21.64	7.6%
A37 - PARKSIDE DRIVE			0.49	4.29	6	3.0	18	159	4.18	1.96	1.20	3.16	200	87.8	0.87	0.98	31.92	9.9%
A38 - SHERWOOD DRIVE			0.94	0.94	14	3.0	42	42	4.33	0.54	0.26	0.80	200	95.0	0.80	0.94	30.60	2.6%
A39 - SHERWOOD DRIVE			0.67	1.61	10	3.0	30	72	4.28	0.91	0.45	1.36	200	96.0	0.40	0.67	21.64	6.3%
A40 - SPRINGSIDE DRIVE			0.63	0.63	14	3.0	42	42	4.33	0.54	0.18	0.71	200	70.6	0.40	0.67	21.64	3.3%
A41 - CONDO			0.97	0.97	40	3.0	120	120	4.22	1.49	0.27	1.77	200	13.6	0.40	0.67	21.64	8.2%
A42 - SPRINGSIDE DRIVE			0.44	2.04	9	3.0	27	189	4.16	2.32	0.57	2.89	200	54.9	0.40	0.67	21.64	13.4%
A43 - SPRINGSIDE DRIVE			0.23	2.27	5	3.0	15	204	4.14	2.50	0.64	3.13	200	23.8	0.50	0.75	24.19	12.9%
A44 - SPRINGSIDE DRIVE			0.11	2.38	2	3.0	6	210	4.14	2.57	0.67	3.23	200	18.5	0.40	0.67	21.64	14.9%
A45 - SPRINGSIDE DRIVE			0.46	2.84	8	3.0	24	234	4.12	2.85	0.80	3.64	200	59.1	0.40	0.67	21.64	16.8%
A46 - SHERWOOD DRIVE			0.48	4.93	6	3.0	18	324	4.06	3.89	1.38	5.27	200	67.7	0.92	1.01	32.82	16.0%
A47 - SHERWOOD DRIVE			0.58	5.51	9	3.0	27	351	4.05	4.19	1.54	5.74	200	56.9	0.88	0.99	32.10	17.9%
A48 - SHERWOOD DRIVE			0.49	6.00	8	3.0	24	375	4.04	4.47	1.68	6.15	200	53.7	1.35	1.23	39.76	15.5%
A49 - SHERWOOD DRIVE			0.30	6.30	4	3.0	12	387	4.03	4.60	1.76	6.37	200	59.1	1.35	1.23	39.76	16.0%
A50 - PARKSIDE DRIVE			0.73	11.32	12	3.0	36	582	3.94	6.77	3.17	9.94	200	86.3	0.40	0.67	21.64	45.9%
A51 - AINTREE PLACE			0.65	0.65	12	3.0	36	36	4.34	0.46	0.18	0.64	200	65.0	1.00	1.06	34.22	1.9%
A52 - PARKSIDE DRIVE			0.76	12.73	15	3.0	45	663	3.91	7.65	3.56	11.21	200	102.5	0.40	0.67	21.64	51.8%
A53 - WESTFIELD PLACE			0.60	0.60	12	3.0	36	36	4.34	0.46	0.17	0.63	200	23.1	1.00	1.06	34.22	1.8%
A54 - WESTFIELD PLACE			0.22	0.82	5	3.0	15	51	4.31	0.65	0.23	0.88	200	43.7	0.40	0.67	21.64	4.1%
A55 - WESTFIELD PLACE			0.23	13.78	5	3.0	15	729	3.88	8.36	3.86	12.22	200	49.2	0.40	0.67	21.64	56.4%
WESTFIELD PLACE				13.78				729	3.88	8.36	3.86	12.22	200	37.6	0.40	0.67	21.64	56.4%
RDS - ROSEDALE			11.85		249	3.0	747	747	3.88	8.55	3.32	11.87						
OXFORD SPS (UCC Calculations)			8.63		56	3.0	168	168	4.17	2.07	2.42	4.49	Current Oxford SPS Flow Rate - UCC Calculated Flows					
EASEMENT - ROSEDALE				25.63				1476	3.68	16.05	7.18	27.71	300	52.4	0.37	0.84	61.36	45.2%
EASEMENT - VAN JON		EXMH 12		25.63				1476	3.68	16.05	7.18	27.71	300	48.8	0.43	0.91	66.15	41.9%
E1 - VAN JON PAVING			1.72						2.00	0.69								
E2 - STONEBRIDGE DR	EXMH 12	EXMH 11	0.14	27.49				1476	3.68	16.05	7.70	28.92	300	28.0	0.29	0.74	54.33	53.2%
E3 - INDUSTRIAL LANDS			0.30						2.00	0.12								
E4 - INDUSTRIAL LANDS			1.82						2.00	0.73								
STONEBRIDGE DR	EXMH 11	EXMH 7		27.49				1476	3.68	16.05	7.70	28.92	300	45.0	0.20	0.62	45.12	64.1%
E5 - INDUSTRIAL LANDS			0.90						2.00	0.36								
E6 - INDUSTRIAL LANDS			4.56						2.00	1.82								
E7 - STONEBRIDGE DR	EXMH 8	EXMH 7	0.29	5.75							1.61	3.79	300	16.0	1.09	1.44	105.32	3.6%
E8 - INDUSTRIAL LANDS		EXMH 7	3.10	3.10					2.00	1.24								
INDUSTRIAL LANDS	EXMH 7	EXMH 6		36.34				1476	3.68	16.05	10.18	34.82	300	88.8	0.20	0.62	45.12	77.2%
INDUSTRIAL LANDS	EXMH 6	EXMH 5		36.34				1476	3.68	16.05	10.18	34.82	300	94.8	0.20	0.62	45.12	77.2%
INDUSTRIAL LANDS	EXMH 5	EXMH 4		36.34				1476	3.68	16.05	10.18	34.82	300	92.6	0.24	0.68	49.42	70.5%
E9 - INDUSTRIAL LANDS		EXMH 4	1.14						2.00	0.46								
E10 - INDUSTRIAL LANDS	EXMH 4	EXMH 3	0.04	37.52				1476	3.68	16.05	10.51	35.61	300	64.7	0.27	0.72	52.42	67.9%
ELM ST DOG PARK	EXMH 3	EXMH 2	0.10	37.62				1476	3.68	16.05	10.53	35.64	300	99.8	0.17	0.57	41.59	85.7%
ELM ST DOG PARK	EXMH 2	EXMH 1	0.12	37.74				1476	3.68	16.05	10.57	35.67	300	120.4	0.21	0.63	46.23	77.2%
ELM ST DOG PARK	EXMH 1	EX 1042	0.01	37.75				1476	3.68	16.05	10.57	35.68	300	14.0	0.22	0.65	47.32	75.4%
ELM ST DOG PARK	EX 1042	EX 1043	0.07	37.82				1476	3.68	16.05	10.59	35.70	300	69.0	0.22	0.65	47.32	75.4%
ELM ST DOG PARK	EX 1043	EX 1062	0.08	37.90				1476	3.68	16.05	10.61	35.72	300	77.0	0.22	0.65	47.32	75.5%



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APPENDIX C

Northland Estates – Stormwater Management Plan

STORMWATER MANAGEMENT PLAN

ROSEDALE SUBDIVISION

CITY OF PORT COLBORNE

Prepared for:

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1510-105 Main Street East
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Prepared by:

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L2W 1A3**

November 23, 2023

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APPENDICES

Appendix A Stormwater Management Facility Calculations

Appendix B MIDUSS Output Files

REFERENCES

1. Stormwater Management Planning and Design Manual
Ontario Ministry of Environment (March 2003)

STORMWATER MANAGEMENT PLAN

ROSEDALE SUBDIVISION

PORT COLBORNE

1.0 INTRODUCTION

1.1 Study Area

The proposed residential subdivision development is located in the City of Port Colborne as part of Lot 30 and Concession 3. As shown on the enclosed Site Location Plan (Figure 1), the subject property is situated east of West Side Road (Highway 58), south of Stonebridge Drive, west of Elm Street, and north of Barrick Road at the north limit of Oxford Boulevard. This Stormwater Management Plan has been completed in support of the application for Draft Plan of Subdivision approval on the subject lands.

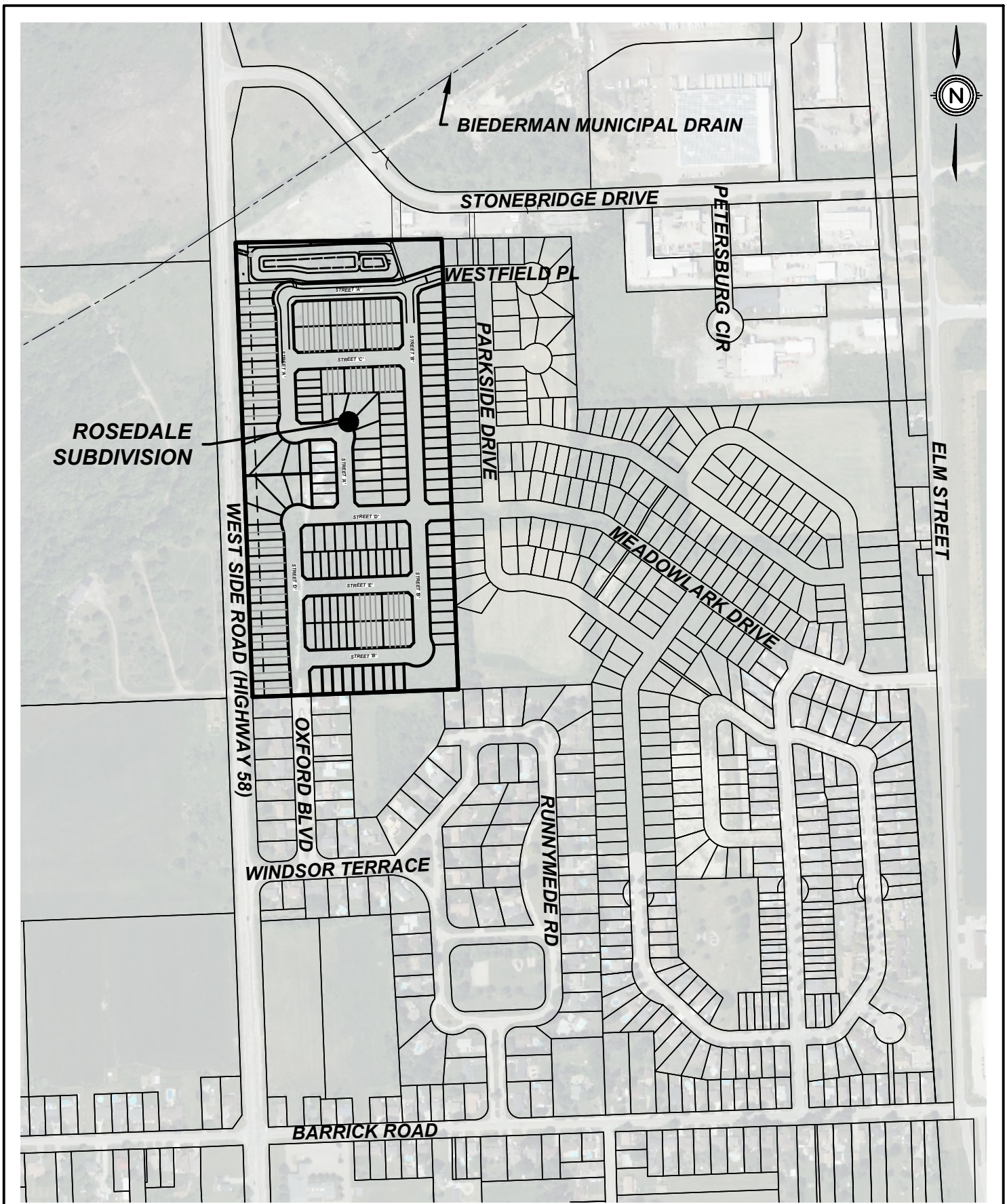
The 12.77-hectare property is bound by existing residential properties on the south side and future residential lands (Meadow Heights Subdivision) to the east, as well as West Side Road (Highway 58) to the west and industrial lands (Van Jon Paving) to the north. The development will have entrances on Oxford Boulevard as well as Meadowlark Drive and Westfield Place as part of the adjacent Meadow Heights subdivision development to the east.

The drainage areas contributing to this Stormwater Management (SWM) Plan will be assessed from the following areas: the subject Rosedale Subdivision lands, the adjacent Meadow Heights Subdivision development, existing residential lands to the south, and a small area of undeveloped agricultural lands on the west side of West Side Road (Highway 58). Future stormwater flows from the development area will discharge to a Stormwater Management (SWM) Facility and subsequent sewer located immediately east of the proposed SWM facility, conveying flows northerly through an easement on the Van John Paving lands to Stonebridge Drive and ultimately the Biederman Drain. This storm sewer will be constructed as part of the adjacent Meadow Heights Subdivision development prior to the Rosedale Subdivision beginning construction.

1.2 Objectives

The objectives of this study are as follows:

1. Establish specific criteria for the management of stormwater from this site.
2. Determine the impact of development on the stormwater peak flow & volume of from this site.
3. Investigate alternatives for controlling the quantity and quality of stormwater from this site.
4. Recommend a comprehensive plan for the management of stormwater during and after construction.



**ROSEDALE
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**CITY OF PORT COLBORNE
SITE LOCATION PLAN**

DATE	2023-10-06
SCALE	1:6000 m
REF No.	5331
DWG No.	FIGURE 1



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Figure 1. Site Location Plan

1.3 Existing & Proposed Conditions

a) Existing Conditions

The development site has been historically been the location of a single detached residential dwelling and associated garage, as well as for agricultural purposes. The gradient of the land is generally north to north-east for the majority of the site directing flows to the north site limit. Flows are then generally directed westerly at the site limit to the West Side Road (Highway 58) MTO road allowance due to the Van Jon Paving development. All stormwater flows from the site ultimately discharge to the Biederman Drain north of the site and to the Welland Recreational Canal further downstream.

The majority of native soil with the study area has been characterized as a Farmington soil with rapid drainage properties though contains shallow bedrock areas close to the surface. The northern portion of the site has been classified with more imperfect to poor draining soils as part of the Franktown soil group.

b) Proposed Conditions

The proposed development will consist of 131 single-detached dwellings and 21 townhouse block (118 units) for a total of 249 residential units. A park will be built at the south-east corner of the site and a stormwater management (SWM) facility will be located at the north limit of the site. The site shall be provided with full municipal services including sanitary sewers, storm sewers, and watermain with asphalt pavement and concrete curbs and gutters.

At this time, due to the current state of approvals and intentions of known developers, it is expected that the adjacent Meadow Heights subdivision development will be constructed prior to the proposed Rosedale Subdivision discussed in this report. It is expected that a storm sewer will be constructed through an easement within the Rosedale Subdivision and northerly-adjacent Van Jon Paving lands to ultimately discharging to the Biederman Drain to provide a stormwater outlet for the Meadow Heights development. As such, calculations and conclusions discussed in this stormwater management plan have been conducted with the assumption that under future conditions, both development sites are fully developed.

2.0 STORMWATER MANAGEMENT CRITERIA

New developments are required to provide stormwater management (SWM) in accordance with provincial and municipal policies including:

- Stormwater Quality Guidelines for New Development (MECP/MNRF, May 1991)
- Stormwater Management Planning and Design Manual (MECP, March 2003)

Based on the comments and outstanding policies from various agencies (City of Port Colborne, Regional Municipality of Niagara, Ministry of Transportation, Niagara Peninsula Conservation Authority (NPCA), and the Ministry of the Environment, Conservation and Parks (MECP), and others) the following site specific considerations were identified:

- The receiving watercourse, Biederman Drain has been identified by the Ministry of Natural Resources watercourse evaluation as a **Type 2 (Important)** fish habitat. Based on this fish habitat, the corresponding MECP level of protection for stormwater management quality practices on all new developments shall be *Normal*.
- The site outlets to the Biederman Drain which contain lands that would be negatively impacted by increased flooding levels, and, therefore, stormwater quantity control is considered necessary to maintain the downstream peak water elevations.

Based on the above policies and site specific considerations, the following stormwater management criteria have been established for this site.

- Stormwater **quality** controls are to be provided for the internal storm system of the Rosedale Subdivision development according to MECP guidelines. It is proposed to provide Normal Protection (70% TSS removal) quality enhancements to the stormwater before discharging to the Biederman Drain.
- Stormwater **quantity** controls are to be provided for the outlet to limit the proposed development peak flows from the 2, 5, 10, 25, 50 and 100 year storm events to existing peak flow levels

3.0 STORMWATER ANALYSIS

A stormwater analysis has been conducted by Upper Canada Consultants as part of the design of the Rosedale Subdivision development using the MIDUSS computer modelling program. A new stormwater analysis was conducted to represent the existing and future conditions to the Biederman Drain.

This program was selected because it is applicable to an urban drainage area like the study area, it is relatively easy to use and modify for the proposed drainage conditions and control facilities, and it readily allows for the use of design storm hyetographs for the various return periods being investigated.

Copies of the current model output files are enclosed in Appendix B.

3.1 Design Storms

Design storm hyetographs were developed using a Chicago distribution based on the Ministry of Transportation’s (MTO) Intensity-Duration-Frequency curves for the subject area in Port Colborne. The MTO’s IDF Curves have been utilized for this development due to the proximity of Highway 58 (West Side Road) immediately adjacent to the site, as the results of this report directly impact their infrastructure. Hyetographs for the 25mm, 2, 5, 10, 25, 50 and 100 year events were developed using a 4-hour Chicago distribution. Table 1 summarizes the rainfall data.

Table 1. Rainfall Data			
Design Storm (Return Period)	Chicago Distribution Parameters		
	a	b	c
25mm	512.000	6.00	0.800
2 Year	397.149	0.0	0.699
5 Year	524.867	0.0	0.699
10 Year	608.845	0.0	0.699
25 Year	715.568	0.0	0.699
50 Year	794.298	0.0	0.699
100 Year	871.279	0.0	0.699
$Intensity \ (mm/hr) = \frac{a}{(t_d + b)^c}$			

3.2 Existing Conditions

The existing conditions were modelled to establish the stormwater peak flows and volumes prior to development within this site. The existing drainage area for this subwatershed is shown on Figure 2. This area was determined from field investigations and recent topographic surveys. Additionally, a schematic outlining the modelling process for both existing and future calculations has been included on Figure 4.

As shown in Figure 2, stormwater flows from an existing agricultural field (Drainage Area ‘FX’) on the west side of West Side Road (Highway 58) are conveyed east under the highway through a 1.2m x 0.9m concrete box culvert and towards the Oxford Boulevard road allowance. Stormwater flows are then captured by a series of catch basins and directed east through a park access and ultimately discharged via culvert to a ditch at the north limit of the park, east of Oxford Boulevard. The ditch passes through the south-east corner of the Rosedale Subdivision lands and through the adjacent Meadow Heights Subdivision lands. The ditch conveys stormwater flows from both Drainage Areas ‘FX’ and ‘WT’ and was included in the original approved engineering design to be accommodated in the Meadow Heights internal storm sewer system.

Through a combination of field surveys and topographical information it has been determined that existing stormwater flows from the Meadow Heights and Rosedale Subdivision lands (Drainage Areas MH and EX respectively) are directed overland westerly at the north limits of the Rosedale Subdivision lands to the Highway 58 road allowance and ultimately to the Biederman Drain at Outlet 'A'.

The adjacent Meadow Heights Subdivision was Draft Approved, Registered and obtained Certificate of Approval for all sewers without the requirement for stormwater management quality or quantity controls prior to discharging to the Biederman Drain. At the time of completing this report, Meadow Heights Phases 1 & 2 have been completed, with a complete engineering submission for the remaining subdivision lands expected to be submitted to the municipality imminently. For the purpose of this report, all calculations have been completed with the assumption that the Meadow Heights subdivision has been completely developed (see figure 2).

Due to unforeseen circumstances however, the location of the storm sewer outlet for the Meadow Heights Subdivision will be adjusted from its' originally planned path north of Parkside Drive. The Meadow Heights Subdivision storm sewer will be constructed within an easement on the Rosedale Subdivision lands, conveying flows westerly on Westfield Place/Street 'A' before being directed north on the east side of the Rosedale SWM facility and continue westerly along the north property line, actively bypassing the future Rosedale Subdivision SWM Facility. The storm sewer will be constructed within an easement through the Van Jon Paving property (#64 Stonebridge Drive and discharge flows via headwall to the Biederman Drain.

An imperviousness of 0.5% has been utilized for both Drainage Areas 'FX' and 'EX' as they are both largely undeveloped vacant properties under existing conditions. An imperviousness of 25.0% has been attributed to Drainage Area 'WT' to align with the single-family residential dwelling and significant park area uses comprising this area. Lastly, an imperviousness of 35.6% has been utilized for the Meadow Heights subdivision which is equivalent to the overall average Runoff Coefficient calculated for the Meadow Heights Subdivision development area per the storm sewer calculations.

Input parameters for the computer model for the existing conditions are shown in Table 2. Table 3 shows the stormwater peak flows and volumes generated by the various design storm events.

3.3 Proposed Conditions

The proposed Rosedale Subdivision development will result in the construction of 249 residential units with an associated park and stormwater management facility. For the purpose of this report, the future imperviousness of the development area has been conservatively increased from 0.5% under existing conditions (Drainage Area EX), to 70.0% under proposed conditions (Drainage Area FUT).

An internal storm sewer system will be constructed to convey stormwater flows up to and including the 5-year design storm event to the stormwater management facility at the north

Stormwater Management Plan
Rosedale Subdivision – City of Port Colborne

limit of the site. As well, stormwater flows unable to enter the storm sewer system during storm events greater than the 5-year event will be directed overland to the stormwater management facility within the future road allowances.

As previously stated, a storm sewer will be constructed immediately east and north of the SWM Facility as part of Meadow Heights stormwater outlet (prior to the Rosedale Subdivision development). The storm sewer will be utilized to convey flows from the stormwater management facility outlet to the Biederman Drain north of the site (Outlet A). This downstream section of storm sewer has been designed to accommodate flows from the Rosedale Subdivision SWM Facility as well as the unrestricted flows from the Meadows Heights Subdivision.

As it will not be ideal to direct major overland flows from the Meadow Heights subdivision through the servicing easement on the Van Jon Paving lands, the roadway design of Street 'A' and Westfield Place at the north limit of the Rosedale/Meadow Heights Subdivision will be designed to direct overland flows from both developments to the proposed SWM facility. During extreme storm events, an emergency overflow spillway will discharge stormwater flows from the SWM facility westerly to the Highway 58 (MTO) road allowance and ultimately to the Biederman Drain (Outlet A). Modelling for the proposed Rosedale Stormwater Management Facility includes overland flows during the 10-100 year storm events.

Ultimately, stormwater flows will continue to discharge flows to Outlet 'A' under future conditions as occurs today under existing conditions.

As the Rosedale Subdivision SWM Facility will accommodate stormwater flows from both the Rosedale (FUT) and Meadow Heights (MH) Subdivisions, modelling has been conducted to determine the peak stormwater flow rates at both the Rosedale Subdivision SWM Facility Outlet as well as the Biederman Drain Outlet (Outlet A) during the larger storm events.

The future drainage areas for the proposed development, shown in Figure 3, were modelled to establish the stormwater peak flows and volumes once development has been completed at the proposed site. Input parameters for the computer model with the proposed development conditions are shown in Table 2.

Table 2. Hydrologic Parameters					
Area No.	Area (ha)	Length (m)	Slope (%)	SCS CN	Percent Impervious
Existing Conditions					
EX	12.77	400	2.0	77	0.5
FX	3.44	150	1.0	77	0.5
WT	10.84	300	1.0	77	25.0
MH	29.25	500	2.0	77	35.7
56.30		Total Area			
Future Conditions					
FUT	12.77	400	2.0	77	70.0
FX	3.44	150	1.0	77	0.5
WT	10.84	300	1.0	77	25.0
MH	29.25	500	2.0	77	35.7
56.30		Total Area			


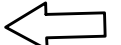

Table 3 below outlines existing peak flows to the Biederman Drain under existing conditions (Outlet A) and combined peak flows to the Biederman Drain under future conditions without stormwater management quantity controls (Outlets A & C). Peak flows and runoff volumes were calculated for the 2-, 5-, 10-, 25-, 50-, and 100-year design storm events.

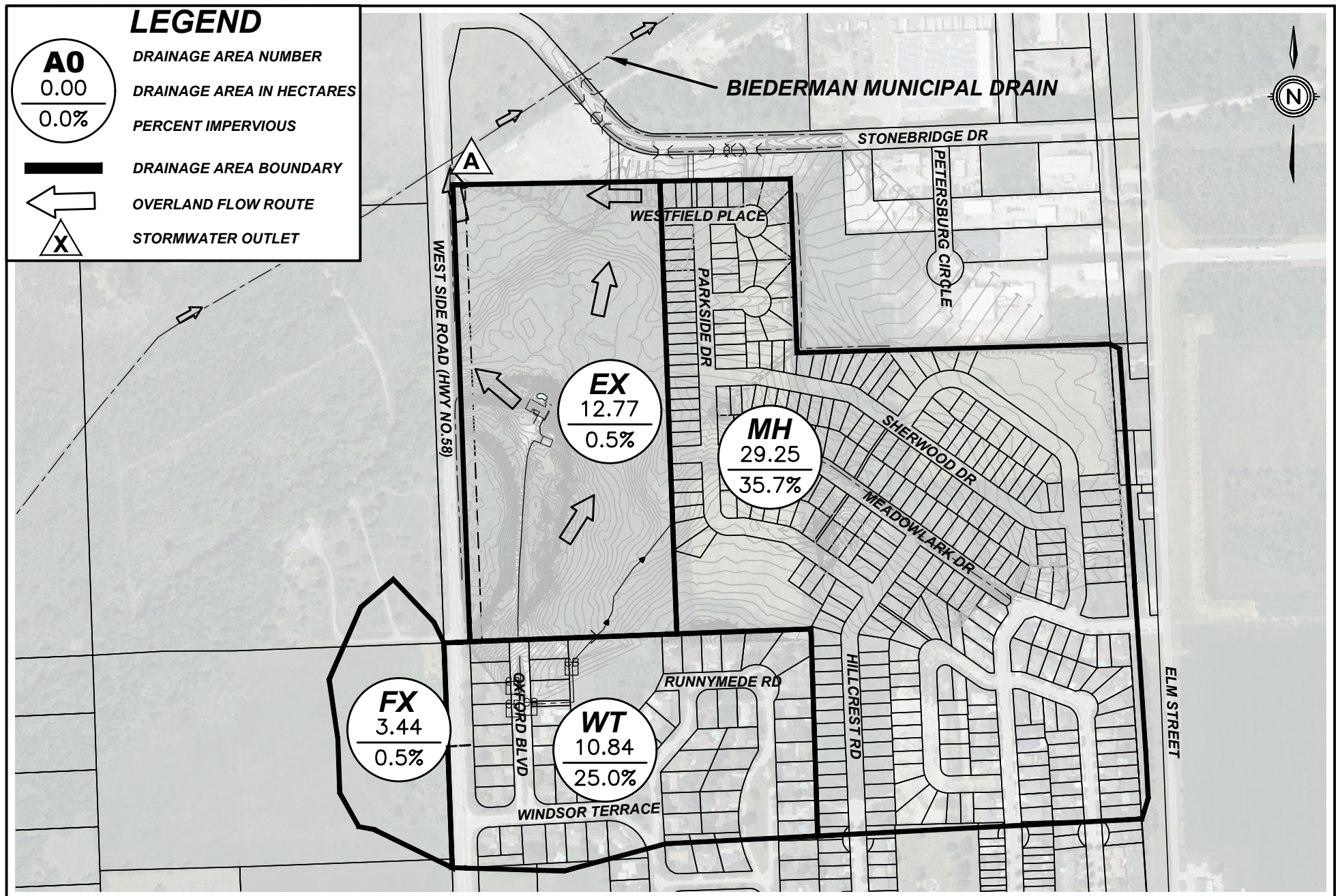
Table 3. Peak Flows and Volumes for Future Development Conditions						
Design Storm	Peak Flow (m³/s)			Volume (m³)		
	Existing	Future*	Change	Existing	Future*	Change
2 Year	1.512	2.697	+ 78%	6,864	8,843	+ 1,979
5 Year	2.224	3.822	+ 72%	10,757	13,207	+ 2,450
10 Year	2.707	4.498	+ 66%	13,539	16,232	+ 2,693
25 Year	3.340	5.425	+ 62%	17,283	20,226	+ 2,943
50 Year	3.824	6.117	+ 60%	20,164	23,257	+ 3,093
100 Year	4.585	7.069	+ 54%	23,078	26,294	+ 3,216

*Note: outlines peak stormwater flows without quantity controls

As seen above in Table 3, stormwater quantity controls are considered necessary for the proposed development since the peak flows and volumes discharging into the Biederman Drain significantly increase as a result of the proposed development. The existing and future stormwater drainage areas shown on Figures 2 and 3 were used to assess the stormwater management plan for this study. A modelling schematic has also been included per Figure 4 to detail how the model was created.

LEGEND

- A0**
DRAINAGE AREA NUMBER
- 0.00
DRAINAGE AREA IN HECTARES
- 0.0%
PERCENT IMPERVIOUS
-  DRAINAGE AREA BOUNDARY
-  OVERLAND FLOW ROUTE
-  STORMWATER OUTLET



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EXISTING OVERALL STORM DRAINAGE AREA PLAN

DATE	2023-09-19
SCALE	1:6000 m
REF No.	5331
DWG No.	FIGURE 2

LEGEND

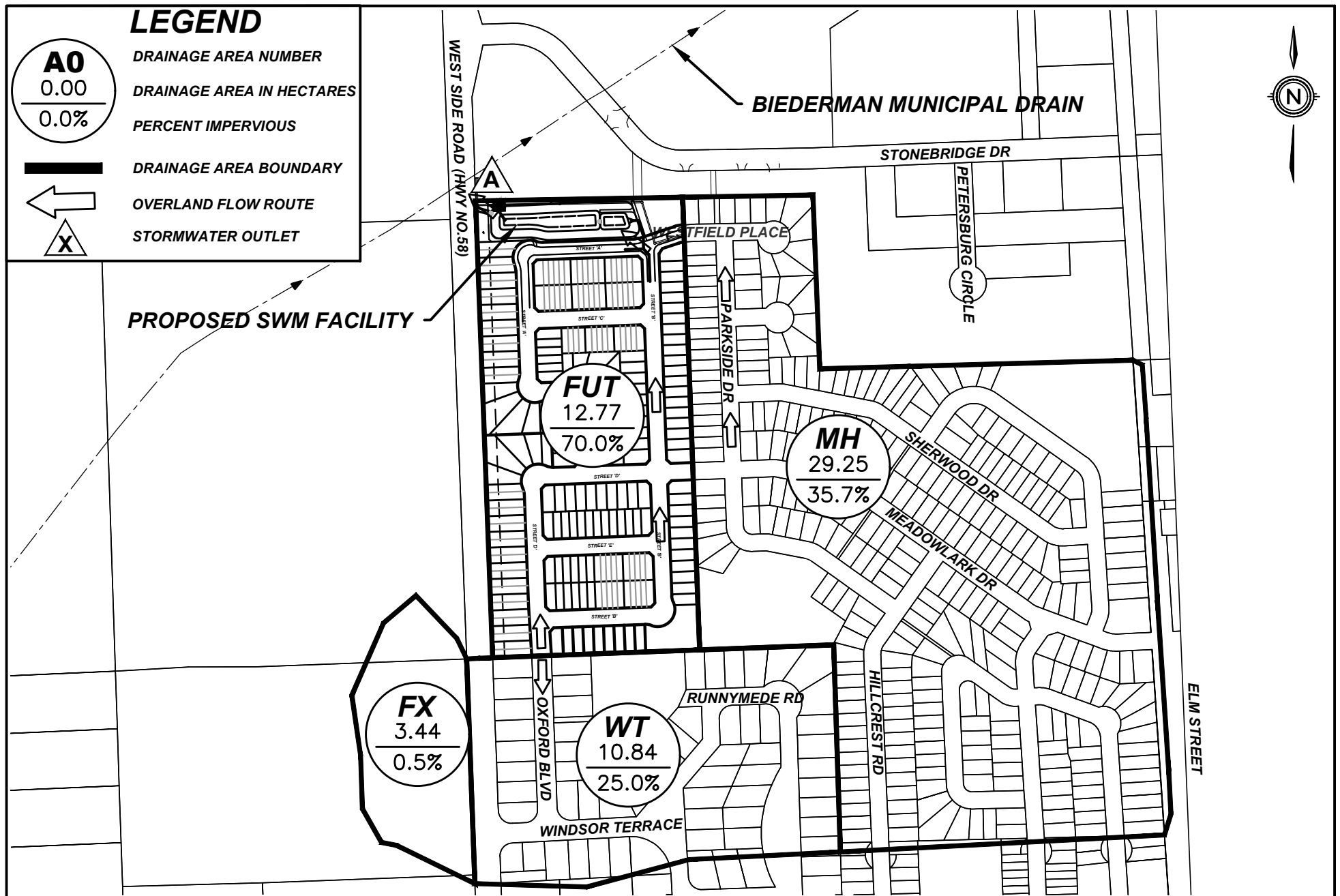
AO
0.00
0.0%

DRAINAGE AREA NUMBER
DRAINAGE AREA IN HECTARES
PERCENT IMPERVIOUS

DRAINAGE AREA BOUNDARY

OVERLAND FLOW ROUTE

STORMWATER OUTLET



PROPOSED SWM FACILITY

BIEDERMAN MUNICIPAL DRAIN

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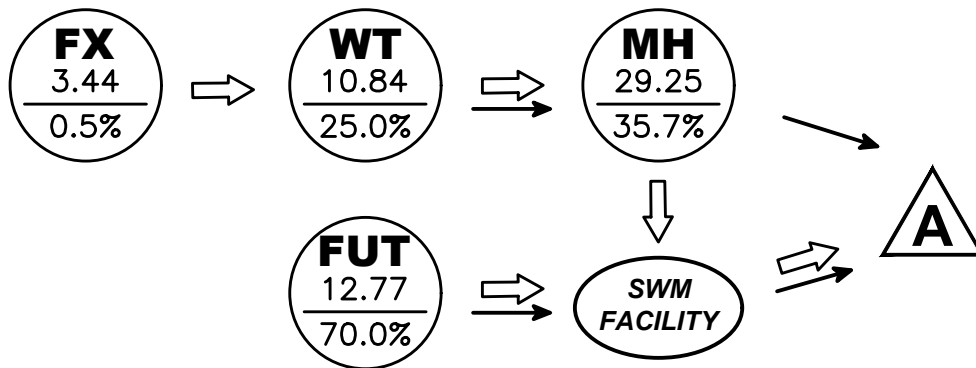
ROSEDALE SUBDIVISION
CITY OF PORT COLBORNE
FUTURE OVERALL STORM DRAINAGE AREA PLAN

DATE	2023-10-06
SCALE	1:6000 m
REF No.	5331
DWG No.	FIGURE 3

EXISTING CONDITIONS

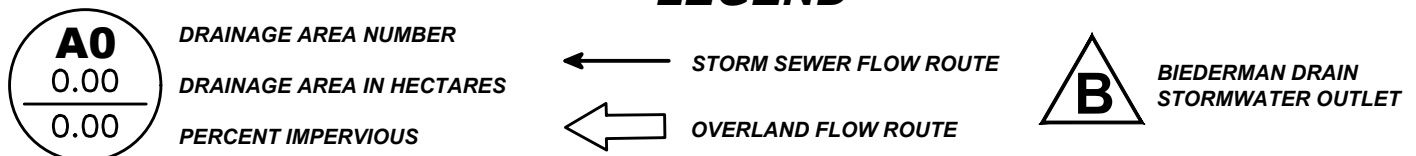


FUTURE CONDITIONS



OUTLET A: BIEDERMAN DRAIN (WEST SIDE ROAD),
 OUTLET B: ROSEDALE SWM FACILITY OUTLET PIPE,
 OUTLET C: BIEDERMAN DRAIN (STONEBRIDGE DRIVE)

LEGEND



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ROSEDALE SUBDIVISION
 CITY OF PORT COLBORNE
SWM MODELLING SCHEMATIC

DATE	2023-10-06
SCALE	N/A
REF No.	5331
DWG No.	FIGURE 4

4.0 STORMWATER MANAGEMENT ALTERNATIVES

4.1 Screening of Stormwater Management Alternatives

A variety of stormwater management alternatives are available to control the quality of stormwater, most of which are described in the Stormwater Management Planning and Design Manual (MECP, March 2003). Alternatives for the proposed and ultimate developments were considered in the following broad categories: lot level, vegetative, infiltration, and end-of-pipe controls. General comments on each category are provided below. Individual alternatives for the proposed development are listed in Table 4 with comments on their effectiveness and applicability to the proposed outlet.

a) Lot Level Controls

Lot level controls are not generally suitable as the primary control facility for quality control. They are generally used to enhance stormwater quality in conjunction with other types of control facilities.

b) Vegetative Alternatives

Vegetative stormwater management practices are not generally suitable as the primary control facility for quality control. They are generally used to enhance stormwater quality in conjunction with other types of control facilities.

c) Infiltration Alternatives

Where soils are suitable, infiltration techniques can be very effective in providing quantity and quality control. However, the very small amount of surface area on this site dedicated to permeable surfaces such as greenspace and landscaping make this an impractical option. Therefore, infiltration techniques will not be considered for this development.

d) End-of-Pipe Alternatives

Surface storage techniques can be very effective in providing quality and quantity control. Dry facilities are effective practices for stormwater erosion and flood control for large drainage areas.

Wet facilities are effective practices for stormwater erosion, quality and quantity control for large drainage areas.

Table 4. Evaluation of Stormwater Management Practices

Rosedale Subdivision	Criteria for Implementation of Stormwater Management Practices (SWMP)					Technical Effectiveness (10 high)	Recommend Implementation Yes / No	Comments
	Topography	Soils	Bedrock	Groundwater	Area			
Site Conditions	Variable 1 to 3%	Silty Sand ±13.3mm/hr	At Considerable Depth	At Considerable Depth	± 12.77ha			
Lot Level Controls								
Lot Grading	<5%	nlc	nlc	nlc	nlc	2	Yes	Quality/quantity benefits
Roof Leaders to Surface	nlc	nlc	nlc	nlc	nlc	2	Yes	Quality/quantity benefits
Roof Ldrs.to Soakaway Pits	nlc	loam, infiltr. > 15 mm/hr	>1m Below Bottom	>1m Below Bottom	< 0.5 ha	6	No	Unsuitable site conditions
Sump Pump Fdtn. Drains	nlc	nlc	nlc	nlc	nlc	2	No	Unsuitable site conditions
Vegetative								
Grassed Swales	< 5 %	nlc	nlc	nlc	nlc	7	Yes	Quality/quantity benefits
Filter Strips(Veg. Buffer)	< 10 %	nlc	nlc	>.5m Below Bottom	< 2 ha	5	No	Unsuitable site conditions
Infiltration								
Infiltration Basins	nlc	loam, infiltr. > 15 mm/hr	>1m Below Bottom	>1m Below Bottom	< 5 ha	2	No	Unsuitable site conditions
Infiltration Trench	nlc	loam, infiltr. > 15 mm/hr	>1m Below Bottom	>1m Below Bottom	< 2 ha	4	No	Unsuitable site conditions
Rear Yard Infiltration	< 2.0 %	loam, infiltr. > 15 mm/hr	>1m Below Bottom	>1m Below Bottom	< 0.5 ha	7	No	Unsuitable site conditions
Perforated Pipes	nlc	loam, infiltr. > 15 mm/hr	>1m Below Bottom	>1m Below Bottom	nlc	4	No	Unsuitable site conditions
Pervious Catch basins	nlc	loam, infiltr. > 15 mm/hr	>1m Below Bottom	>1m Below Bottom	nlc	3	No	Unsuitable site conditions
Sand Filters	nlc	nlc	nlc	>.5m Below Bottom	< 5 ha	5	No	High maintenance/poor aesthetics
Surface Storage								
Dry Ponds	nlc	nlc	nlc	nlc	> 5 ha	7	No	No quality control
Wet Ponds	nlc	nlc	nlc	nlc	> 5 ha	9	Yes	Very effective quality control
Wetlands	nlc	nlc	nlc	nlc	> 5 ha	10	No	Very effective quality control
Other								
Oil/Grit Separator	nlc	nlc	nlc	nlc	<2 ha	3	No	Limited benefit/area too large

Reference: Stormwater Management Practices Planning and Design Manual - 1994
 nlc - No Limiting Criteria

4.2 Selection of Stormwater Management Alternatives

Stormwater management alternatives were screened based on technical effectiveness, physical suitability for this site, and their ability to meet the stormwater management criteria established for proposed and future development areas. The following stormwater management alternatives are recommended for implementation on the proposed development:

- **Lot grading** to be kept as flat as practical in order to slow down stormwater and encourage infiltration.
- **Roof leaders to be discharged to the ground surface** in order to slow down stormwater and encourage infiltration.
- **Grassed swales** to be used to collect rear lot drainage. Grassed swales tend to filter sediments and slow down the rate of stormwater.
- A **wet pond facility** to be constructed to provide stormwater quality enhancement for frequent storms.

5.0 STORMWATER MANAGEMENT PLAN

A MIDUSS model was created to assess existing, future and ultimate development peak flows and stormwater volumes generated by the proposed subdivision. The stormwater management facility was sized according to MECP Guidelines (MECP, March 2003) as follows:

5.1 Proposed Stormwater Management Facility

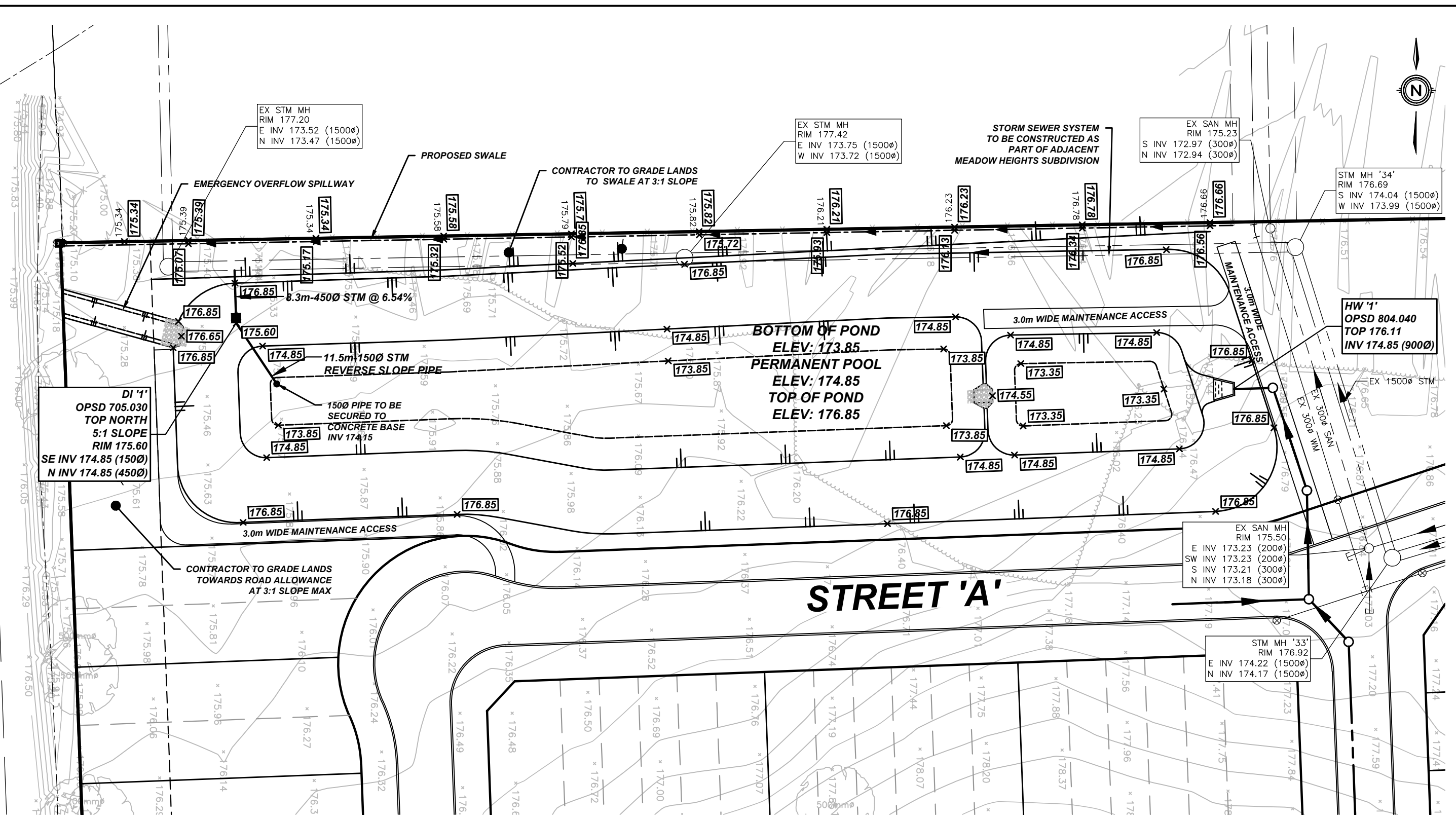
5.1.1 Stormwater Quality

The stormwater drainage outlet for the proposed development is the Biederman Drain, which has been identified by the Ministry of Natural Resources watercourse evaluation as a Type 2 fish habitat. Based on this fish habitat, the corresponding MECP level of protection for stormwater management quality practices on all new developments shall be Normal.

Based on Table 3.2 of SWMP & Design Manual, the water quality storage requirement is approximately 130m³/ha for *Normal* protection for developments with 70% impervious areas. The drainage area requiring stormwater quality improvement draining to the proposed facility is 12.77 hectares. The storage volumes required for this proposed facility are shown in Table 5.



WEST SIDE ROAD
(HIGHWAY 58)



ROSEDALE SUBDIVISION

CITY OF PORT COLBORNE

PROPOSED STORMWATER MANAGEMENT FACILITY DETAIL

DATE	2023-11-23
SCALE	1:600 m
REF No.	5331
DWG No.	FIGURE 5

Table 5. Stormwater Quality Volume Calculations	
<p>Total Water Quality Volume = 12.77 ha x 130 m³/ha = 1,660 m³</p>	
<p>Reference: Table 3.2, SWMP & Design Manual (MECP 2003)</p>	
<p>Minimum Permanent Pool Volume = 12.77 ha x 90 m³/ha = 1,149 m³</p>	<p>Minimum Extended Detention Volume = 12.77 ha x 40 m³/ha = 511 m³</p>

As per the Stormwater Management Facility Calculations in Appendix A, the proposed stormwater management facility will have a Permanent Pool volume of 1,693m³ as well as an extended detention volume of 2,746m³. These are both greater than the minimum required.

5.1.2 Stormwater Quantity Control

As shown in the previous Table 3, stormwater management quantity controls are required to reduce the peak flows from the development area to existing conditions for up to and including the 100-year design storm event. The stormwater peak flows from the proposed development and surrounding lands shall be reduced to the existing levels by providing stormwater quantity storage. It is proposed to construct a control structure outlet to reduce the peak stormwater flows discharging from the proposed facility.

As described previously, overland flows during storm events greater than the 5-year event from the Rosedale Subdivision development area as well as the adjacent Meadow Heights Subdivision and upstream lands shall be directed proposed stormwater management facility. Modelling for the proposed Rosedale Stormwater Management Facility includes overland flow volumes during the 10-100 year storm events.

5.1.3 Stormwater Management Facility Configuration

As seen on the proposed Stormwater Management Facility detail (Figure 5), the layout of the SWM facility is providing a single storm sewer outlet to the future easement storm sewer from Meadow Heights.

It is proposed to construct a three-stage outlet for the stormwater management facility as shown in Figure 5. The first stage of control consists of a reverse slope pipe acting as a 150mm diameter orifice to provide the required quality controls. The second stage of control consists of a ditch inlet catch basin and outlet pipe which provides an outlet for flows exceeding the extended detention volume. An emergency spillway will complete the third stage providing an outlet for flows exceeding the capacity of the ditch inlet catch basin and outlet pipe during extreme storm events.

The proposed effective bottom elevation of the facility is 173.85m, and the permanent pool water level is 174.85m for a water depth of 1.0 metre. The configuration of the facility provides 1,693m³ of permanent pool volume, which is more than the required 1,149m³. The ditch inlet will be constructed at an elevation of 175.60m providing an extended detention of 2,746m³, greater than the 511m³ required. The proposed top of pond is at an elevation of 176.85m which will provide a total active volume of 9,663m³.

Stormwater Management Plan
Rosedale Subdivision, City of Port Colborne

Based on the configuration of the proposed facility, it was determined that a 150mm diameter quality orifice shall provide approximately 28 hours of detention for the 25mm design storm event (24 hours is the minimum).

The outflow pipe from the stormwater management facility is to be 450mm in diameter and will convey stormwater flows from the ditch inlet and quality pipe to 1500mm diameter storm sewer which will be constructed immediately north of the SWM Facility as part of the Meadow Heights Subdivision stormwater outlet. A stage-storage-discharge relationship was determined for the facility and is included in Appendix A for reference purposes.

As the facility will be discharging flows from multiple areas, a comparison of flows from existing to future conditions for specifically the Rosedale Subdivision development will not be attainable. Therefore, Table 6 below outlines the characteristics of the SWM facility during all storm events, though Table 7 on the following page outlines the overall peak stormwater flows discharging to the Biederman Drain.

Design Storm (Return Period)	Peak Flows (m³/s)		Maximum Elevation	Maximum Volume (m³)
	Inflow	Outflow		
25mm	0.821	0.028	175.31	1,562
2 Year	1.342	0.040	175.59	2,711
5 Year	1.643	0.072	175.73	3,327
10 Year	1.991	0.083	175.87	4,001
25 Year	2.918	0.083	176.11	5,254
50 Year	3.610	0.083	176.29	6,247
100 Year	4.562	0.083	176.52	7,568

Based on the MIDUSS model, Table 6 shows the maximum wet pond elevation of 176.52m, and an active storage volume of 7,568 m³ for the 100-year design storm event. Therefore, as the SWM facility has a top elevation of 176.85m, a freeboard of 0.33m will be provided by this Stormwater Management Plan.

During all storm events, stormwater flows from the development area are ultimately conveyed towards Outlet 'A' (West Side Road, MTO road allowance) under existing conditions. An emergency overflow spillway has been included as part of the SWM Facility design, discharging flows towards the West Side Road MTO road allowance. However, due to the size of the SWM Facility, no stormwater flows will be conveyed to the MTO road allowance as part of Outlet 'A' (West Side Road) during any of the modelled storm events.

The storm sewer system immediately downstream of the SWM facility outlet to the Biederman Drain was designed to convey peak stormwater flows up to and including the 5-year design storm event. During the 5-year event, the Rosedale SWM Facility will discharge approximately 72L/s to the downstream storm sewer system according to the MIDUSS modelling. As part of the design of this storm sewer, a conservatively increased flow allocation from the Rosedale SWM Facility of 100L/s was included in the calculations

Stormwater Management Plan
Rosedale Subdivision, City of Port Colborne

to ensure sufficient capacity was provided. With this allocation, the sewers experience flows reaching approximately 87% of their capacity during the 5-year event.

During events greater than the 5-year storm event, it has been conservatively assumed that storm sewers can accommodate flow at an additional 15% on top of their full flow capacity due to surcharged conditions. Therefore, for the purpose of modelling the stormwater management facility, a maximum discharge rate of 83 L/s (72L/s + 15%) has been utilized for flows being discharged at the outlet pipe. Additional outflow capacity is included once stormwater flows within the SWM facility reach the spillway elevation of 176.65m.

Table 7 details the difference in peak stormwater flows ultimately discharging to the Biederman Drain at Outlet A under existing conditions as well as to the Biederman Drain at Stonebridge Drive (Outlet C) under future conditions with the stormwater management facility in place.

Design Storm	Peak Flow (m³/s)		
	Existing	Future with SWM	Change*
2 Year	1.512	1.512	0.0%
5 Year	2.224	2.206	- 0.8%
10 Year	2.707	2.540	- 6.2%
25 Year	3.340	2.545	- 23.8%
50 Year	3.824	2.590	-32.3%
100 Year	4.585	2.589	- 43.5%

Note: *indicates the percent change between existing conditions and future conditions with stormwater management controls in place.

Therefore, as outlined in Table 7 above, stormwater flows discharging to the Biederman Drain will remain relatively unchanged during storm events up to and including the 5-year event, and experience significant peak flow reductions as a result of the proposed stormwater management plan during storms greater than the 5-year event. As discussed previously, it should be noted again that overland flows from the adjacent Meadow Heights Subdivision during storms greater than the 5-year event will be directed to the Rosedale SWM Facility and ultimately be provided quantity controls as a result.

The proposed facility has a single storm sewer inlet, therefore, the sediment forebay was designed to minimize the transport of heavy sediment from the storm sewer outlet throughout the facility and to localize maintenance activities. Calculations for the forebay sizing follow MECP Guidelines and are shown in Tables 8 for the storm sewer outlet.

Table 8. Stormwater Management Facility Forebay Sizing		
a) Forebay Settling Length (MOECC SWMP&D, Equation 4.5)		
$\text{Settling Length} = \sqrt{\frac{r * Q_p}{V_s}}$	r = 2.3 :1	(Length:Width Ratio)
	Q _p = 0.03 m ³ /s	(25mm Storm Pond Discharge)
	V _s = 0.0003 m/s	(Settling Velocity)
Settling Length = 15.22 m		
b) Dispersion Length (MOECC SWMP&D, Equation 4.6)		
$\text{Dispersion Length} = \frac{8 * Q}{D * V_f}$	Q = 1.643 m ³ /s	(5 Yr Stm Sew Design Inflow)
	D = 1.50 m	(Depth of Forebay)
	V _f = 0.5 m/s	(Desired Velocity)
Dispersion Length = 17.53 M		
c) Minimum Forebay Deep Zone Bottom Width (MOECC SWMP&D, Equation 4.7)		
$\text{Width} = \frac{\text{Dispersion Length}}{8}$	Minimum Forebay Length from Equations 3.3 and 3.4 17.53 m (minimum required length)	
Width = 2.19 m (minimum required width)		
d) Average Velocity of Flow		
$\text{Average Velocity} = \frac{Q}{A}$	Q = 0.839 m ³ /s	(Quality Design Inflow)
	A = 21.00 m ²	(Cross Sectional Area)
	D = 1.50 m	(Depth of Forebay)
	W = 9.50 m	(Proposed Bottom Width)
	S = 3 :1	(Side slopes - minimum)
Average Velocity = 0.04 m/s		
Is this Acceptable? Yes (Maximum velocity of flow = 0.15 m/s)		
e) Cleanout Frequency		
Is this Acceptable? Yes	L = 22.0 m	(Proposed Bottom Length)
	ASL = 2.8 m ³ /ha	(Annual Sediment Loading)
	A = 12.77 ha	(Drainage Area)
	FRC = 70 %	(Facility Removal Efficiency)
	FV = 586.9 m ³	(Forebay Volume)
Cleanout Frequency = 11.5 years		
Is this Acceptable? Yes (10 year minimum cleanout frequency)		

6.0 SEDIMENT AND EROSION CONTROL

Sediment and erosion controls are required during all construction phases of this development to limit the transport of sediment into the Biederman Drain.

The following additional erosion and sediment controls will also be implemented during construction:

- Install silt control fencing along the limits of construction of the development to collect sediment in overland flows before discharging to downstream systems. The silt control fence installed along east end of site will be installed along the wetland buffer to act as the limit of construction.
- Re-vegetate disturbed areas as soon as possible after grading works have been completed.
- Lot grading and siltation controls plans will be provided with sediment and erosion control measures to the appropriate agencies for approval during the final design stage.

7.0 STORMWATER MANAGEMENT FACILITY MAINTENANCE

7.1 Wetpond Facility

Maintenance is a necessary and important aspect of urban stormwater quality and quantity measures such as constructed wetlands. Many pollutants (ie. nutrients, metals, bacteria, etc.) bind to sediment and therefore removal of sediment on a scheduled basis is required.

The wet pond for this development is subject to frequent wetting and deposition of sediments as a result of frequent low intensity storm events. The purpose of the wet pond is to improve post development sediment and contaminant loadings by detaining the 'first flush' flow for a 24 hour period. For the initial operation period of the stormwater management facility, the required frequency of maintenance is not definitively known and many of the maintenance tasks will be performed on an 'as required' basis. For example, during the home construction phase of the development there will be a greater potential for increased maintenance frequency, which depends on the effectiveness of sediment and erosion control techniques employed.

Inspections of the wet pond will indicate whether or not maintenance is required. Inspections should be made after every significant storm during the first two years of operation or until all development is completed to ensure the wet pond is functioning properly. This may translate into an average of six inspections per year. Once all building activity is finalized, inspections shall be performed annually. The following points should be addressed during inspections of the facility.

- a) Standing water above the inlet storm sewer invert a day or more after a storm may

- indicate a blockage in the reverse slope pipe or orifice. The blockage may be caused by trash or sediment and a visual inspection would be required to determine the cause.
- b) The vegetation around the wet pond should be inspected to ensure its function and aesthetics. Visual inspections will indicate whether replacement of plantings are required. A decline in vegetation habitat may indicate that other aspects of the constructed wet pond are operating improperly, such as the detention times may be inadequate or excessive.
 - c) The accumulation of sediment and debris at the wet pond inlet sediment forebay or around the high water line of the wet pond should be inspected. This will indicate the need for sediment removal or debris clean up.
 - d) The wet pond has been created by excavating a detention area. The integrity of the embankments should be periodically checked to ensure that it remains watertight and the side slopes have not sloughed.

Grass cutting is a maintenance activity that is done solely for aesthetic purposes. It is recommended that grass cutting be eliminated. It should be noted that municipal by-laws may require regular grass maintenance for weed control.

Trash removal is an integral part of maintenance and an annual cleanup, usually in the spring, is a minimum requirement. After this, trash removal is performed as required basis on observation of trash build-up during inspections.

To ensure long term effectiveness, the sediment that accumulates in the forebay area should be removed periodically to ensure that sediment is not deposited throughout the facility. For sediment removal operations, typical grading/excavating equipment should be used to remove sediment from the inlet forebay and detention areas. Care should be taken to ensure that limited damage occurs to existing vegetation and habitat.

Generally the sediment which is removed from the detention pond will not be contaminated to the point that it would be classified as hazardous waste. However, the sediment should be tested to determine the disposal options.

8.0 CONCLUSIONS AND RECOMMENDATIONS

Based on the findings of this study, the following conclusions are offered:

- Infiltration techniques are not suitable for this site as the primary control facility due to the low soil infiltration rates and the large drainage area for this development.
- The proposed stormwater management facility will provide stormwater quality controls for the proposed Rosedale Subdivision and quantity controls for the Rosedale Subdivision as well as the adjacent Meadow Heights Subdivision during larger storm events.
- Various lot level vegetative stormwater management practices can be implemented to enhance stormwater quality.
- This report was prepared in accordance with the provincial guidelines contained in "Stormwater Management Planning and Design Manual, March 2003".

The above conclusions lead to the following recommendations:

- That the stormwater management criteria established in this report be accepted.
- That a stormwater management wet pond facility be constructed to provide stormwater quality protection to MECP *Normal* Protection levels and quantity controls as outlined in this report.
- That additional lot level controls and vegetative stormwater management practices as described previously in this report be implemented.

Prepared By:



Kurt Tiessen, E.I.T.



Reviewed By:



Jason Schooley, P.Eng.
November 23, 2023

APPENDICES

APPENDIX A
Stormwater Management Facility Calculations

Upper Canada Consultants
 30 HANNOVER DRIVE, UNIT 3
 St. Catharines, Ontario L2W 1A3

DATE: SEPTEMBER 2023

PROJECT NAME: ROSEDALE SUBDIVISION
 PROJECT NO.: 5331

STORMWATER MANAGEMENT FACILITY WETPOND

Quality Requirements	Quality Orifice	Ditch Inlet Weir	Outflow Pipe Orifice	Overflow Spillway
Drainage Area (ha) = 12.77	Diameter (m) = 0.150	Length (m) = 0.60	Diameter (m) = 0.450	Minor Length (m) = 3.00
Normal (m ³ /ha) = 130	(@ 70%) Cd = 0.63	Width (m) = 0.60	Cd = 0.63	Slopes (X:1) = 3.00
Perm Pool (m ³ /ha) = 90	Invert (m) = 174.85	Grate Slope (X:1) = 4	Invert (m) = 174.85	Minor Invert (m) = 176.65
Perm Pool Vol (m ³) = 1,149		Inlet Elevation (m) = 175.60	Overt (m) = 175.30	Major Invert (m) = 0.00
Active Vol (m ³) 511		Cd = 1.84		Major Invert (m) = 176.85
25mm MOEE (m ³) m ³				MOE Equation 4.10 Drawdown Coefficient 'C2' = 1,945
Perm. Pool Elev. = 174.85 m				MOE Equation 4.10 Drawdown Coefficient 'C3' = 2,939
				MOE Equation 4.10 Drawdown Time (h) = 28.7

Elevation	Increment Depth (m)	Active Depth (m)	Surface Area (m ²)	Average Surface Area (m ²)	Increment Volume (m ³)	Permanent Volume (m ³)	Active Volume (m ³)	Quality Orifice (m ³ /s)	Ditch Inlet (m ³ /s)	Max Pipe Orifice (m ³ /s)	Max Outflow (5yr+15%) (m ³ /s)	Overflow Spillway (m ³ /s)	Total Outflow (m ³ /s)	Average Discharge (m ³ /s)	Side Slope (H:V)
173.85		-1.00	1,077			0									
	0.50			1,380	690										
174.35		-0.50	1,683			690									
	0.50			2,006	1,003										
174.85		0.00	2,329			1,693								0.00	PERM
	0.00			2,634	0										
174.85		0.00	2,939				0.0	0.000	0.000	0.00		0.00	0.00	0.016	PERM
	0.50			3,425	1,713										5:1
175.35		0.50	3,911				1712.6	0.031	0.000	0.198		0.000	0.031	0.024	5:1
	0.25			4,135	1,034										
175.60		0.75	4,359				2746.4	0.040	0.000	0.298		0.000	0.040	0.067	5:1
	0.16			4,505	721										
175.76		0.91	4,651				3467.2	0.044	0.035	0.347		0.000	0.080	0.081	5:1
	0.09			4,734	426										
175.85		1.00	4,817				3893.3	0.047	0.069	0.371	0.083	0.000	0.083	0.083	5:1
	0.50			5,289	2,645										
176.35		1.50	5,762				6538.0	0.058	0.359	0.486	0.083	0.000	0.083	0.083	5:1
	0.30			6,055	1,816										
176.65		1.80	6,348				8354.4	0.064	0.594	0.544	0.083	0.000	0.083	0.158	5:1
	0.10			6,447	645										
176.75		1.90	6,546				8999.1	0.066	0.681	0.561	0.083	0.150	0.233	0.353	5:1
	0.10			6,646	665										
176.85		2.00	6,746				9663.7	0.068	0.771	0.579	0.083	0.390	0.473		

- Notes**
- Quality Orifice flow is the orifice controlling for the 24 hour detention period and uses an orifice formula.
 - Pipe Orifice flow is calculated using an orifice formula on the pipe from the ditch inlet to the outlet and uses the total head on the orifice.
 - Overflow Weir flow is calculated using a trapezoidal weir to convey outflow for less frequent storms through the embankment with an emergency spillway.
 - Total Outflow is calculated by adding the Overflow Spillway with the lowest of Quality Orifice plus Ditch Inlet or Max Pipe Orifice.

APPENDIX B
MIDUSS Output Files

Existing Conditions

Output File (4.7) EX.OUT opened 2023-09-22 9:56
 Units used are defined by G = 9.810
 24 144 10.000 are MAXDT MAXHYD & DTMIN values
 Licensee: UPPER CANADA CONSULTANTS

35 COMMENT
 4 line(s) of comment
 ROSEDALE SUBDIVISION
 STORMWATER MANAGEMENT PLAN
 EXISTING CONDITIONS TO BIEDERMAN DRAIN
 OCTOBER 2022

35 COMMENT
 1 line(s) of comment
 UTILIZED FULL SITE AREA
 START

14 1 1=Zero; 2=Define

35 COMMENT
 3 line(s) of comment

 * 25MM DESIGN STORM EVENT *

2 STORM
 1 1=Chicago;2=Huff;3=User;4=Cdnlhr;5=Historic
 512.000 Coefficient a
 6.000 Constant b (min)
 .800 Exponent c
 .450 Fraction to peak r
 240.000 Duration 6 240 min
 25.035 mm Total depth

3 IMPERVIOUS
 1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
 .015 Manning "n"
 98.000 SCS Curve No or C
 .100 Ia/S Coefficient
 .518 Initial Abstraction

35 COMMENT
 1 line(s) of comment
 *** ROSEDALE - DRAINAGE AREA EX ***

4 CATCHMENT
 1.000 ID No.6 99999
 12.770 Area in hectares
 400.000 Length (PERV) metres
 2.000 Gradient (%)
 .500 Per cent Impervious
 400.000 Length (IMPERV)
 .000 %Imp. with Zero Dpth
 1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
 .250 Manning "n"
 77.000 SCS Curve No or C
 .100 Ia/S Coefficient
 7.587 Initial Abstraction
 1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
 .024 .000 .000 .000 c.m/s
 .130 .799 .134 C perv/imperv/total

27 HYDROGRAPH DISPLAY
 4 is # of Hyeto/Hydrograph chosen
 Volume = .4272098E+03 c.m

15 ADD RUNOFF
 .024 .024 .000 .000 c.m/s

9 ROUTE
 .000 Conduit Length
 .000 No Conduit defined
 .000 Zero lag
 .000 Beta weighting factor
 .000 Routing timestep
 0 No. of sub-reaches
 .024 .024 .024 .000 c.m/s

17 COMBINE
 3 Junction Node No.
 .024 .024 .024 .024 c.m/s

14 START
 1 1=Zero; 2=Define

35 COMMENT
 1 line(s) of comment
 *** FIELD - DRAINAGE AREA FX ***

4 CATCHMENT
 1.000 ID No.6 99999
 3.440 Area in hectares
 150.000 Length (PERV) metres
 1.000 Gradient (%)
 .500 Per cent Impervious
 150.000 Length (IMPERV)
 .000 %Imp. with Zero Dpth
 1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
 .250 Manning "n"
 77.000 SCS Curve No or C
 .100 Ia/S Coefficient
 7.587 Initial Abstraction
 1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
 .009 .000 .024 .024 c.m/s
 .130 .804 .134 C perv/imperv/total

15 ADD RUNOFF
 .009 .009 .024 .024 c.m/s

11 CHANNEL
 .300 Base Width =
 3.000 Left bank slope 1:
 3.000 Right bank slope 1:
 .030 Manning's "n"
 .500 O/a Depth in metres
 1.000 Select Grade in %
 Depth = .052 metres
 Velocity = .373 m/sec
 Flow Capacity = 1.222 c.m/s
 Critical depth = .039 metres

9 ROUTE
 400.000 Conduit Length
 .493 Supply X-factor <.5
 401.782 Supply K-lag (sec)
 .500 Beta weighting factor
 600.000 Routing timestep
 2 No. of sub-reaches
 .009 .009 .009 .024 c.m/s

16 NEXT LINK
 .009 .009 .009 .024 c.m/s

35 COMMENT
 1 line(s) of comment
 *** EXISTING RESIDENTIAL - DRAINAGE AREA WT ***

4 CATCHMENT
 1.000 ID No.6 99999

10.840 Area in hectares
 300.000 Length (PERV) metres
 1.000 Gradient (%)
 25.000 Per cent Impervious
 300.000 Length (IMPERV)
 .000 %Imp. with Zero Dpth
 1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
 .250 Manning "n"
 77.000 SCS Curve No or C
 .100 Ia/S Coefficient
 7.587 Initial Abstraction
 1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
 .248 .009 .009 .024 c.m/s
 .130 .802 .298 C perv/imperv/total

15 ADD RUNOFF
 .248 .249 .009 .024 c.m/s

11 CHANNEL
 .300 Base Width =
 3.000 Left bank slope 1:
 3.000 Right bank slope 1:
 .030 Manning's "n"
 .500 O/a Depth in metres
 1.000 Select Grade in %
 Depth = .256 metres
 Velocity = .909 m/sec
 Flow Capacity = 1.222 c.m/s
 Critical depth = .224 metres

9 ROUTE
 200.000 Conduit Length
 .472 Supply X-factor <.5
 164.970 Supply K-lag (sec)
 .500 Beta weighting factor
 150.000 Routing timestep
 1 No. of sub-reaches
 .248 .249 .207 .024 c.m/s

16 NEXT LINK
 .248 .207 .207 .024 c.m/s

35 COMMENT
 1 line(s) of comment
 *** MEADOW HEIGHTS - DRAINAGE AREA MH ***

4 CATCHMENT
 1.000 ID No.6 99999
 29.250 Area in hectares
 500.000 Length (PERV) metres
 2.000 Gradient (%)
 35.700 Per cent Impervious
 500.000 Length (IMPERV)
 .000 %Imp. with Zero Dpth
 1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
 .250 Manning "n"
 77.000 SCS Curve No or C
 .100 Ia/S Coefficient
 7.587 Initial Abstraction
 1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
 .928 .207 .207 .024 c.m/s
 .130 .806 .372 C perv/imperv/total

15 ADD RUNOFF
 .928 1.135 .207 .024 c.m/s

27 HYDROGRAPH DISPLAY
 5 is # of Hyeto/Hydrograph chosen
 Volume = .3644621E+04 c.m

8 PIPE
 .500 Minimum velocity m/sec
 2.920 Maximum velocity m/sec
 .013 Pipe Manning's "n"
 1.350 Diameter in metres
 .600 Select Grade in %
 Depth = .484 metres
 Velocity = 2.464 m/sec
 Pipe Capacity = 4.134 c.m/s
 Critical depth= .558 metres

9 ROUTE
 500.000 Conduit Length
 .455 Supply X-factor <.5
 152.187 Supply K-lag (sec)
 .500 Beta weighting factor
 150.000 Routing timestep
 1 No. of sub-reaches
 .928 1.135 .943 .024 c.m/s

17 COMBINE
 3 Junction Node No.
 .928 1.135 .943 .951 c.m/s

18 CONFLUENCE
 3 Junction Node No.
 .928 .951 .943 .000 c.m/s

27 HYDROGRAPH DISPLAY
 5 is # of Hyeto/Hydrograph chosen
 Volume = .4069800E+04 c.m

14 START
 1 1=Zero; 2=Define

35 COMMENT
 3 line(s) of comment

 * MTO 2 YEAR DESIGN STORM EVENT *

2 STORM
 1 1=Chicago;2=Huff;3=User;4=Cdnlhr;5=Historic
 397.149 Coefficient a
 .000 Constant b (min)
 .699 Exponent c
 .450 Fraction to peak r
 240.000 Duration 6 240 min
 34.451 mm Total depth

3 IMPERVIOUS
 1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
 .015 Manning "n"
 98.000 SCS Curve No or C
 .100 Ia/S Coefficient
 .518 Initial Abstraction

35 COMMENT
 1 line(s) of comment
 *** ROSEDALE - DRAINAGE AREA EX ***

4 CATCHMENT
 1.000 ID No.6 99999
 12.770 Area in hectares
 400.000 Length (PERV) metres
 2.000 Gradient (%)
 .500 Per cent Impervious
 400.000 Length (IMPERV)
 .000 %Imp. with Zero Dpth
 1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat

.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.063 .000 .943 .000 c.m/s
.204 .850 .207 C perv/imperv/total

27 HYDROGRAPH DISPLAY
4 is # of Hyeto/Hydrograph chosen
Volume = .9111658E+03 c.m

15 ADD RUNOFF
.063 .063 .943 .000 c.m/s

9 ROUTE
.000 Conduit Length
.500 Supply X-factor <.5
.000 Supply K-lag (sec)
.500 Beta weighting factor
600.000 Routing timestep
1 No. of sub-reaches
.063 .063 .063 .000 c.m/s

17 COMBINE
3 Junction Node No.
.063 .063 .063 .063 c.m/s

14 START
1 1=Zero; 2=Define

35 COMMENT
1 line(s) of comment
*** FIELD - DRAINAGE AREA FX ***

4 CATCHMENT
1.000 ID No.6 99999
3.440 Area in hectares
150.000 Length (PERV) metres
1.000 Gradient (%)
.500 Per cent Impervious
150.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.023 .000 .063 .063 c.m/s
.204 .841 .207 C perv/imperv/total

15 ADD RUNOFF
.023 .023 .063 .063 c.m/s

11 CHANNEL
.300 Base Width =
3.000 Left bank slope 1:
3.000 Right bank slope 1:
.030 Manning's "n"
.500 O/a Depth in metres
1.000 Select Grade in %
Depth = .084 metres
Velocity = .488 m/sec
Flow Capacity = 1.222 c.m/s
Critical depth = .067 metres

9 ROUTE
400.000 Conduit Length
.489 Supply X-factor <.5
307.501 Supply K-lag (sec)
.500 Beta weighting factor
600.000 Routing timestep
2 No. of sub-reaches
.023 .023 .023 .063 c.m/s

16 NEXT LINK
.023 .023 .023 .063 c.m/s

35 COMMENT
1 line(s) of comment
*** EXISTING RESIDENTIAL - DRAINAGE AREA WT ***

4 CATCHMENT
1.000 ID No.6 99999
10.840 Area in hectares
300.000 Length (PERV) metres
1.000 Gradient (%)
25.000 Per cent Impervious
300.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.367 .023 .023 .063 c.m/s
.204 .849 .365 C perv/imperv/total

15 ADD RUNOFF
.367 .370 .023 .063 c.m/s

11 CHANNEL
.300 Base Width =
3.000 Left bank slope 1:
3.000 Right bank slope 1:
.030 Manning's "n"
.500 O/a Depth in metres
1.000 Select Grade in %
Depth = .304 metres
Velocity = 1.006 m/sec
Flow Capacity = 1.222 c.m/s
Critical depth = .270 metres

9 ROUTE
200.000 Conduit Length
.468 Supply X-factor <.5
149.160 Supply K-lag (sec)
.500 Beta weighting factor
150.000 Routing timestep
1 No. of sub-reaches
.367 .370 .325 .063 c.m/s

16 NEXT LINK
.367 .325 .325 .063 c.m/s

35 COMMENT
1 line(s) of comment
*** MEADOW HEIGHTS - DRAINAGE AREA MH ***

4 CATCHMENT
1.000 ID No.6 99999
29.250 Area in hectares
500.000 Length (PERV) metres
2.000 Gradient (%)
35.700 Per cent Impervious
500.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat

.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
1.385 .325 .325 .063 c.m/s
.204 .841 .431 C perv/imperv/total

15 ADD RUNOFF
1.385 1.710 .325 .063 c.m/s

27 HYDROGRAPH DISPLAY
5 is # of Hyeto/Hydrograph chosen
Volume = .5955855E+04 c.m

8 PIPE
.500 Minimum velocity m/sec
2.920 Maximum velocity m/sec
.013 Pipe Manning's "n"
1.350 Diameter in metres
.600 Select Grade in %
Depth = .605 metres
Velocity = 2.750 m/sec
Pipe Capacity = 4.134 c.m/s
Critical depth = .692 metres

9 ROUTE
500.000 Conduit Length
.442 Supply X-factor <.5
136.363 Supply K-lag (sec)
.500 Beta weighting factor
150.000 Routing timestep
1 No. of sub-reaches
1.385 1.710 1.493 .063 c.m/s

17 COMBINE
3 Junction Node No.
1.385 1.710 1.493 1.512 c.m/s

18 CONFLUENCE
3 Junction Node No.
1.385 1.512 1.493 .000 c.m/s

27 HYDROGRAPH DISPLAY
5 is # of Hyeto/Hydrograph chosen
Volume = .6864000E+04 c.m

14 START
1 1=Zero; 2=Define

35 COMMENT
3 line(s) of comment

* MTO 5 YEAR DESIGN STORM EVENT *

2 STORM
1 1=Chicago;2=Huff;3=User;4=Cdnlhr;5=Historic
524.867 Coefficient a
.000 Constant b (min)
.699 Exponent c
.450 Fraction to peak r
240.000 Duration 6 240 min
45.530 mm Total depth

3 IMPERVIOUS
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.015 Manning "n"
98.000 SCS Curve No or C
.100 Ia/S Coefficient
.518 Initial Abstraction

35 COMMENT
1 line(s) of comment
*** ROSEDAILE - DRAINAGE AREA EX ***

4 CATCHMENT
1.000 ID No.6 99999
12.770 Area in hectares
400.000 Length (PERV) metres
2.000 Gradient (%)
.500 Per cent Impervious
400.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.147 .000 1.493 .000 c.m/s
.278 .883 .281 C perv/imperv/total

27 HYDROGRAPH DISPLAY
4 is # of Hyeto/Hydrograph chosen
Volume = .1632299E+04 c.m

15 ADD RUNOFF
.147 .147 1.493 .000 c.m/s

9 ROUTE
.000 Conduit Length
.500 Supply X-factor <.5
.000 Supply K-lag (sec)
.500 Beta weighting factor
600.000 Routing timestep
1 No. of sub-reaches
.147 .147 .147 .000 c.m/s

17 COMBINE
3 Junction Node No.
.147 .147 .147 .147 c.m/s

14 START
1 1=Zero; 2=Define

35 COMMENT
1 line(s) of comment
*** FIELD - DRAINAGE AREA FX ***

4 CATCHMENT
1.000 ID No.6 99999
3.440 Area in hectares
150.000 Length (PERV) metres
1.000 Gradient (%)
.500 Per cent Impervious
150.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.055 .000 .147 .147 c.m/s
.278 .859 .280 C perv/imperv/total

15 ADD RUNOFF
.055 .055 .147 .147 c.m/s

11 CHANNEL
.300 Base Width =
3.000 Left bank slope 1:

```

3.000 Right bank slope 1:
.030 Manning's "n"
.500 O/a Depth in metres
1.000 Select Grade in %
Depth = .129 metres
Velocity = .616 m/sec
Flow Capacity = 1.222 c.m/s
Critical depth = .106 metres
9 ROUTE
400.000 Conduit Length
.492 Supply X-factor <.5
487.040 Supply K-lag (sec)
.500 Beta weighting factor
300.000 Routing timestep
1 No. of sub-reaches
.055 .055 .053 .147 c.m/s
16 NEXT LINK
.055 .053 .053 .147 c.m/s
35 COMMENT
1 line(s) of comment
*** EXISTING RESIDENTIAL - DRAINAGE AREA WT ***
4 CATCHMENT
1.000 ID No.6 99999
10.840 Area in hectares
300.000 Length (PERV) metres
1.000 Gradient (%)
25.000 Per cent Impervious
300.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.515 .053 .053 .147 c.m/s
.278 .884 .429 C perv/imperv/total
15 ADD RUNOFF
.515 .525 .053 .147 c.m/s
11 CHANNEL
.300 Base Width =
3.000 Left bank slope 1:
3.000 Right bank slope 1:
.030 Manning's "n"
.500 O/a Depth in metres
1.000 Select Grade in %
Depth = .352 metres
Velocity = 1.098 m/sec
Flow Capacity = 1.222 c.m/s
Critical depth = .317 metres
9 ROUTE
200.000 Conduit Length
.463 Supply X-factor <.5
136.564 Supply K-lag (sec)
.500 Beta weighting factor
120.000 Routing timestep
1 No. of sub-reaches
.515 .525 .476 .147 c.m/s
16 NEXT LINK
.515 .476 .476 .147 c.m/s
35 COMMENT
1 line(s) of comment
*** MEADOW HEIGHTS - DRAINAGE AREA MH ***
4 CATCHMENT
1.000 ID No.6 99999
29.250 Area in hectares
500.000 Length (PERV) metres
2.000 Gradient (%)
35.700 Per cent Impervious
500.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
1.941 .476 .476 .147 c.m/s
.278 .882 .493 C perv/imperv/total
15 ADD RUNOFF
1.941 2.416 .476 .147 c.m/s
27 HYDROGRAPH DISPLAY
5 is # of Hyeto/Hydrograph chosen
Volume = .9128701E+04 c.m
8 PIPE
.500 Minimum velocity m/sec
2.920 Maximum velocity m/sec
.013 Pipe Manning's "n"
1.350 Diameter in metres
.600 Select Grade in %
Depth = .741 metres
Velocity = 3.000 m/sec
Pipe Capacity = 4.134 c.m/s
Critical depth= .829 metres
9 ROUTE
500.000 Conduit Length
.424 Supply X-factor <.5
124.986 Supply K-lag (sec)
.500 Beta weighting factor
120.000 Routing timestep
1 No. of sub-reaches
1.941 2.416 2.180 .147 c.m/s
17 COMBINE
3 Junction Node No.
1.941 2.416 2.180 2.224 c.m/s
18 CONFLUENCE
3 Junction Node No.
1.941 2.224 2.180 .000 c.m/s
27 HYDROGRAPH DISPLAY
5 is # of Hyeto/Hydrograph chosen
Volume = .1075680E+05 c.m
14 START
1 1=Zero; 2=Define
35 COMMENT
3 line(s) of comment
*****
* MTO 10 YEAR DESIGN STORM EVENT *
*****
2 STORM
1 1=Chicago;2=Huff;3=User;4=Cdnlhr;5=Historic
608.845 Coefficient a
.000 Constant b (min)
.699 Exponent c
.450 Fraction to peak r
240.000 Duration 6 240 min
52.815 mm Total depth
3 IMPERVIOUS
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.015 Manning "n"
98.000 SCS Curve No or C
.100 Ia/S Coefficient
.518 Initial Abstraction
35 COMMENT
1 line(s) of comment
*** ROSSDALE - DRAINAGE AREA EX ***
4 CATCHMENT
1.000 ID No.6 99999
12.770 Area in hectares
400.000 Length (PERV) metres
2.000 Gradient (%)
.500 Per cent Impervious
400.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.225 .000 2.180 .000 c.m/s
.320 .897 .322 C perv/imperv/total
27 HYDROGRAPH DISPLAY
4 is # of Hyeto/Hydrograph chosen
Volume = .2174500E+04 c.m
15 ADD RUNOFF
.225 .225 2.180 .000 c.m/s
9 ROUTE
.000 Conduit Length
.500 Supply X-factor <.5
.000 Supply K-lag (sec)
.500 Beta weighting factor
600.000 Routing timestep
1 No. of sub-reaches
.225 .225 .225 .000 c.m/s
17 COMBINE
3 Junction Node No.
.225 .225 .225 .225 c.m/s
14 START
1 1=Zero; 2=Define
35 COMMENT
1 line(s) of comment
*** FIELD - DRAINAGE AREA FX ***
4 CATCHMENT
1.000 ID No.6 99999
3.440 Area in hectares
150.000 Length (PERV) metres
1.000 Gradient (%)
.500 Per cent Impervious
150.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.079 .000 .225 .225 c.m/s
.320 .878 .322 C perv/imperv/total
15 ADD RUNOFF
.079 .079 .225 .225 c.m/s
11 CHANNEL
.300 Base Width =
3.000 Left bank slope 1:
3.000 Right bank slope 1:
.030 Manning's "n"
.500 O/a Depth in metres
1.000 Select Grade in %
Depth = .154 metres
Velocity = .679 m/sec
Flow Capacity = 1.222 c.m/s
Critical depth = .129 metres
9 ROUTE
400.000 Conduit Length
.491 Supply X-factor <.5
441.992 Supply K-lag (sec)
.500 Beta weighting factor
300.000 Routing timestep
1 No. of sub-reaches
.079 .079 .077 .225 c.m/s
16 NEXT LINK
.079 .077 .077 .225 c.m/s
35 COMMENT
1 line(s) of comment
*** EXISTING RESIDENTIAL - DRAINAGE AREA WT ***
4 CATCHMENT
1.000 ID No.6 99999
10.840 Area in hectares
300.000 Length (PERV) metres
1.000 Gradient (%)
25.000 Per cent Impervious
300.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.613 .077 .077 .225 c.m/s
.320 .897 .464 C perv/imperv/total
15 ADD RUNOFF
.613 .632 .077 .225 c.m/s
11 CHANNEL
.300 Base Width =
3.000 Left bank slope 1:
3.000 Right bank slope 1:
.030 Manning's "n"
.500 O/a Depth in metres
1.000 Select Grade in %
Depth = .381 metres
Velocity = 1.150 m/sec
Flow Capacity = 1.222 c.m/s

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Critical depth = .344 metres

9 ROUTE
 200.000 Conduit Length
 .460 Supply X-factor <.5
 130.387 Supply K-lag (sec)
 .500 Beta weighting factor
 120.000 Routing timestep
 1 No. of sub-reaches
 .613 .632 .579 .225 c.m/s

16 NEXT LINK
 .613 .579 .579 .225 c.m/s

35 COMMENT
 1 line(s) of comment
 *** MEADOW HEIGHTS - DRAINAGE AREA MH ***

4 CATCHMENT
 1.000 ID No.6 99999
 29.250 Area in hectares
 500.000 Length (PERV) metres
 2.000 Gradient (%)
 35.700 Per cent Impervious
 500.000 Length (IMPERV)
 .000 %Imp. with Zero Dpth
 1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
 .250 Manning "n"
 77.000 SCS Curve No or C
 .100 Ia/S Coefficient
 7.587 Initial Abstraction
 1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
 2.305 .579 .579 .225 c.m/s
 .320 .898 .526 C perv/imperv/total

15 ADD RUNOFF
 2.305 2.884 .579 .225 c.m/s

27 HYDROGRAPH DISPLAY
 5 is # of Hyeto/Hydrograph chosen
 Volume = .1137058E+05 c.m

8 PIPE
 .500 Minimum velocity m/sec
 2.920 Maximum velocity m/sec
 .013 Pipe Manning's 'n'
 1.350 Diameter in metres
 .600 Select Grade in %
 Depth = .830 metres
 Velocity = 3.123 m/sec
 Pipe Capacity = 4.134 c.m/s
 Critical depth= .908 metres

9 ROUTE
 500.000 Conduit Length
 .407 Supply X-factor <.5
 120.096 Supply K-lag (sec)
 .500 Beta weighting factor
 120.000 Routing timestep
 1 No. of sub-reaches
 2.305 2.884 2.637 .225 c.m/s

17 COMBINE
 3 Junction Node No.
 2.305 2.884 2.637 2.707 c.m/s

18 CONFLUENCE
 3 Junction Node No.
 2.305 2.707 2.637 .000 c.m/s

27 HYDROGRAPH DISPLAY
 5 is # of Hyeto/Hydrograph chosen
 Volume = .1353900E+05 c.m

14 START
 1 1=Zero; 2=Define

35 COMMENT
 3 line(s) of comment

 * MTD 25 YEAR DESIGN STORM EVENT *

2 STORM
 1 1=Chicago;2=Huff;3=User;4=Cdnlhr;5=Historic
 715.568 Coefficient a
 .000 Constant b (min)
 .699 Exponent c
 .450 Fraction to peak r
 240.000 Duration 6 240 min
 62.073 mm Total depth

3 IMPERVIOUS
 1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
 .015 Manning "n"
 98.000 SCS Curve No or C
 .100 Ia/S Coefficient
 .518 Initial Abstraction

35 COMMENT
 1 line(s) of comment
 *** ROSEDALE - DRAINAGE AREA EX ***

4 CATCHMENT
 1.000 ID No.6 99999
 12.770 Area in hectares
 400.000 Length (PERV) metres
 2.000 Gradient (%)
 .500 Per cent Impervious
 400.000 Length (IMPERV)
 .000 %Imp. with Zero Dpth
 1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
 .250 Manning "n"
 77.000 SCS Curve No or C
 .100 Ia/S Coefficient
 7.587 Initial Abstraction
 1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
 .331 .000 2.637 .000 c.m/s
 .367 .910 .370 C perv/imperv/total

27 HYDROGRAPH DISPLAY
 4 is # of Hyeto/Hydrograph chosen
 Volume = .2929079E+04 c.m

15 ADD RUNOFF
 .331 .331 2.637 .000 c.m/s

9 ROUTE
 .000 Conduit Length
 .500 Supply X-factor <.5
 .000 Supply K-lag (sec)
 .500 Beta weighting factor
 600.000 Routing timestep
 1 No. of sub-reaches
 .331 .331 .331 .000 c.m/s

17 COMBINE
 3 Junction Node No.
 .331 .331 .331 .331 c.m/s

14 START
 1 1=Zero; 2=Define

35 COMMENT

1 line(s) of comment
 *** FIELD - DRAINAGE AREA FX ***

4 CATCHMENT
 1.000 ID No.6 99999
 3.440 Area in hectares
 150.000 Length (PERV) metres
 1.000 Gradient (%)
 .500 Per cent Impervious
 150.000 Length (IMPERV)
 .000 %Imp. with Zero Dpth
 1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
 .250 Manning "n"
 77.000 SCS Curve No or C
 .100 Ia/S Coefficient
 7.587 Initial Abstraction
 1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
 .127 .000 .331 .331 c.m/s
 .367 .898 .369 C perv/imperv/total

15 ADD RUNOFF
 .127 .127 .331 .331 c.m/s

11 CHANNEL
 .300 Base Width =
 3.000 Left bank slope 1:
 3.000 Right bank slope 1:
 .030 Manning's "n"
 .500 O/a Depth in metres
 1.000 Select Grade in %
 Depth = .190 metres
 Velocity = .766 m/sec
 Flow Capacity = 1.222 c.m/s
 Critical depth = .162 metres

9 ROUTE
 400.000 Conduit Length
 .489 Supply X-factor <.5
 391.534 Supply K-lag (sec)
 .500 Beta weighting factor
 300.000 Routing timestep
 1 No. of sub-reaches
 .127 .127 .122 .331 c.m/s

16 NEXT LINK
 .127 .122 .122 .331 c.m/s

35 COMMENT
 1 line(s) of comment
 *** EXISTING RESIDENTIAL - DRAINAGE AREA WT ***

4 CATCHMENT
 1.000 ID No.6 99999
 10.840 Area in hectares
 300.000 Length (PERV) metres
 1.000 Gradient (%)
 25.000 Per cent Impervious
 300.000 Length (IMPERV)
 .000 %Imp. with Zero Dpth
 1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
 .250 Manning "n"
 77.000 SCS Curve No or C
 .100 Ia/S Coefficient
 7.587 Initial Abstraction
 1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
 .742 .122 .122 .331 c.m/s
 .367 .911 .503 C perv/imperv/total

15 ADD RUNOFF
 .742 .775 .122 .331 c.m/s

11 CHANNEL
 .300 Base Width =
 3.000 Left bank slope 1:
 3.000 Right bank slope 1:
 .030 Manning's "n"
 .500 O/a Depth in metres
 1.000 Select Grade in %
 Depth = .415 metres
 Velocity = 1.211 m/sec
 Flow Capacity = 1.222 c.m/s
 Critical depth = .377 metres

9 ROUTE
 200.000 Conduit Length
 .457 Supply X-factor <.5
 123.848 Supply K-lag (sec)
 .500 Beta weighting factor
 120.000 Routing timestep
 1 No. of sub-reaches
 .742 .775 .720 .331 c.m/s

16 NEXT LINK
 .742 .720 .720 .331 c.m/s

35 COMMENT
 1 line(s) of comment
 *** MEADOW HEIGHTS - DRAINAGE AREA MH ***

4 CATCHMENT
 1.000 ID No.6 99999
 29.250 Area in hectares
 500.000 Length (PERV) metres
 2.000 Gradient (%)
 35.700 Per cent Impervious
 500.000 Length (IMPERV)
 .000 %Imp. with Zero Dpth
 1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
 .250 Manning "n"
 77.000 SCS Curve No or C
 .100 Ia/S Coefficient
 7.587 Initial Abstraction
 1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
 2.767 .720 .720 .331 c.m/s
 .367 .911 .561 C perv/imperv/total

15 ADD RUNOFF
 2.767 3.486 .720 .331 c.m/s

27 HYDROGRAPH DISPLAY
 5 is # of Hyeto/Hydrograph chosen
 Volume = .1435864E+05 c.m

8 PIPE
 .500 Minimum velocity m/sec
 2.920 Maximum velocity m/sec
 .013 Pipe Manning's 'n'
 1.350 Diameter in metres
 .600 Select Grade in %
 Depth = .950 metres
 Velocity = 3.238 m/sec
 Pipe Capacity = 4.134 c.m/s
 Critical depth= .999 metres

9 ROUTE
 500.000 Conduit Length
 .377 Supply X-factor <.5
 115.797 Supply K-lag (sec)

```

.500 Beta weighting factor
120.000 Routing timestep
1 No. of sub-reaches
2.767 3.486 3.226 .331 c.m/s
17 COMBINE
3 Junction Node No.
2.767 3.486 3.226 3.340 c.m/s
18 CONFLUENCE
3 Junction Node No.
2.767 3.340 3.226 .000 c.m/s
27 HYDROGRAPH DISPLAY
5 is # of Hyeto/Hydrograph chosen
Volume = .1728300E+05 c.m
14 START
1 1-Zero; 2-Define
35 COMMENT
3 line(s) of comment
*****
* MTO 50 YEAR DESIGN STORM EVENT *
*****
2 STORM
1 1=Chicago;2=Huff;3=User;4=Cdnlhr;5=Historic
794.298 Coefficient a
.000 Constant b (min)
.699 Exponent c
.450 Fraction to peak r
240.000 Duration 6 240 min
68.903 mm Total depth
3 IMPERVIOUS
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.015 Manning "n"
98.000 SCS Curve No or C
.100 Ia/S Coefficient
.518 Initial Abstraction
35 COMMENT
1 line(s) of comment
*** ROSEDALE - DRAINAGE AREA EX ***
4 CATCHMENT
1.000 ID No.6 99999
12.770 Area in hectares
400.000 Length (PERV) metres
2.000 Gradient (%)
.500 Per cent Impervious
400.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Triangl; 2=Rectangl; 3=SWM HYD; 4=Lin. Reserv
.431 .000 3.226 .000 c.m/s
.398 .915 .400 C perv/imperv/total
27 HYDROGRAPH DISPLAY
4 is # of Hyeto/Hydrograph chosen
Volume = .3521674E+04 c.m
15 ADD RUNOFF
.431 .431 3.226 .000 c.m/s
9 ROUTE
.000 Conduit Length
.500 Supply X-factor <.5
.000 Supply K-lag (sec)
.500 Beta weighting factor
600.000 Routing timestep
1 No. of sub-reaches
.431 .431 .431 .000 c.m/s
17 COMBINE
3 Junction Node No.
.431 .431 .431 .431 c.m/s
14 START
1 1-Zero; 2-Define
35 COMMENT
1 line(s) of comment
*** FIELD - DRAINAGE AREA FX ***
4 CATCHMENT
1.000 ID No.6 99999
3.440 Area in hectares
150.000 Length (PERV) metres
1.000 Gradient (%)
.500 Per cent Impervious
150.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Triangl; 2=Rectangl; 3=SWM HYD; 4=Lin. Reserv
.161 .000 .431 .431 c.m/s
.397 .909 .400 C perv/imperv/total
15 ADD RUNOFF
.161 .161 .431 .431 c.m/s
11 CHANNEL
.300 Base Width =
3.000 Left bank slope 1:
3.000 Right bank slope 1:
.030 Manning's "n"
.500 O/a Depth in metres
1.000 Select Grade in %
Depth = .211 metres
Velocity = .814 m/sec
Flow Capacity = 1.222 c.m/s
Critical depth = .182 metres
9 ROUTE
400.000 Conduit Length
.488 Supply X-factor <.5
368.744 Supply K-lag (sec)
.500 Beta weighting factor
300.000 Routing timestep
1 No. of sub-reaches
.161 .161 .154 .431 c.m/s
16 NEXT LINK
.161 .154 .154 .431 c.m/s
35 COMMENT
1 line(s) of comment
*** EXISTING RESIDENTIAL - DRAINAGE AREA WT ***
4 CATCHMENT
1.000 ID No.6 99999
10.840 Area in hectares
300.000 Length (PERV) metres
1.000 Gradient (%)
25.000 Per cent Impervious
300.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient

```

7.587 Initial Abstraction
 1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
 .550 .000 3.669 .000 c.m/s
 .425 .919 .427 C perv/imperv/total

27 HYDROGRAPH DISPLAY
 4 is # of Hyeto/Hydrograph chosen
 Volume = .4124768E+04 c.m

15 ADD RUNOFF
 .550 .550 3.669 .000 c.m/s

9 ROUTE
 .000 Conduit Length
 .500 Supply X-factor <.5
 .000 Supply K-lag (sec)
 .500 Beta weighting factor
 600.000 Routing timestep
 1 No. of sub-reaches
 .550 .550 .550 .000 c.m/s

17 COMBINE
 3 Junction Node No.
 .550 .550 .550 .550 c.m/s

14 START
 1 1=Zero; 2=Define

35 COMMENT
 1 line(s) of comment
 *** FIELD - DRAINAGE AREA FX ***

4 CATCHMENT
 1.000 ID No.6 99999
 3.440 Area in hectares
 150.000 Length (PERV) metres
 1.000 Gradient (%)
 .500 Per cent Impervious
 150.000 Length (IMPERV)
 .000 %Imp. with Zero Dpth
 1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
 .250 Manning "n"
 77.000 SCS Curve No or C
 .100 Ia/S Coefficient
 7.587 Initial Abstraction
 1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
 .196 .000 .550 .550 c.m/s
 .425 .917 .427 C perv/imperv/total

15 ADD RUNOFF
 .196 .196 .550 .550 c.m/s

11 CHANNEL
 .300 Base Width =
 3.000 Left bank slope 1:
 3.000 Right bank slope 1:
 .030 Manning's "n"
 .500 O/a Depth in metres
 1.000 Select Grade in %
 Depth = .231 metres
 Velocity = .856 m/sec
 Flow Capacity = 1.222 c.m/s
 Critical depth = .200 metres

9 ROUTE
 400.000 Conduit Length
 .487 Supply X-factor <.5
 350.564 Supply K-lag (sec)
 .500 Beta weighting factor
 300.000 Routing timestep
 1 No. of sub-reaches
 .196 .196 .186 .550 c.m/s

16 NEXT LINK
 .196 .186 .186 .550 c.m/s

35 COMMENT
 1 line(s) of comment
 *** EXISTING RESIDENTIAL - DRAINAGE AREA WT ***

4 CATCHMENT
 1.000 ID No.6 99999
 10.840 Area in hectares
 300.000 Length (PERV) metres
 1.000 Gradient (%)
 25.000 Per cent Impervious
 300.000 Length (IMPERV)
 .000 %Imp. with Zero Dpth
 1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
 .250 Manning "n"
 77.000 SCS Curve No or C
 .100 Ia/S Coefficient
 7.587 Initial Abstraction
 1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
 .924 .186 .186 .550 c.m/s
 .425 .922 .549 C perv/imperv/total

15 ADD RUNOFF
 .924 .988 .186 .550 c.m/s

11 CHANNEL
 .300 Base Width =
 3.000 Left bank slope 1:
 3.000 Right bank slope 1:
 .030 Manning's "n"
 .500 O/a Depth in metres
 1.000 Select Grade in %
 Depth = .458 metres
 Velocity = 1.287 m/sec
 Flow Capacity = 1.222 c.m/s
 Critical depth = .420 metres

9 ROUTE
 200.000 Conduit Length
 .453 Supply X-factor <.5
 116.540 Supply K-lag (sec)
 .500 Beta weighting factor
 120.000 Routing timestep
 1 No. of sub-reaches
 .924 .988 .929 .550 c.m/s

16 NEXT LINK
 .924 .929 .929 .550 c.m/s

35 COMMENT
 1 line(s) of comment
 *** MEADOW HEIGHTS - DRAINAGE AREA MH ***

4 CATCHMENT
 1.000 ID No.6 99999
 29.250 Area in hectares
 500.000 Length (PERV) metres
 2.000 Gradient (%)
 35.700 Per cent Impervious
 500.000 Length (IMPERV)
 .000 %Imp. with Zero Dpth
 1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat

.250 Manning "n"
 77.000 SCS Curve No or C
 .100 Ia/S Coefficient
 7.587 Initial Abstraction
 1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
 3.453 .929 .929 .550 c.m/s
 .425 .926 .604 C perv/imperv/total

15 ADD RUNOFF
 3.453 4.381 .929 .550 c.m/s

27 HYDROGRAPH DISPLAY
 5 is # of Hyeto/Hydrograph chosen
 Volume = .1895659E+05 c.m

8 PIPE
 .500 Minimum velocity m/sec
 2.920 Maximum velocity m/sec
 .013 Pipe Manning's "n"
 1.350 Diameter in metres
 .600 Select Grade in %
 Surcharged HGL= .674 %
 Velocity = 3.061 m/sec
 Pipe Capacity = 4.134 c.m/s
 Critical depth= 1.113 metres

9 ROUTE
 500.000 Conduit Length
 .500 Supply X-factor <.5
 .000 Supply K-lag (sec)
 .500 Beta weighting factor
 600.000 Routing timestep
 1 No. of sub-reaches
 3.453 4.381 4.381 .550 c.m/s

17 COMBINE
 3 Junction Node No.
 3.453 4.381 4.381 4.585 c.m/s

18 CONFLUENCE
 3 Junction Node No.
 3.453 4.585 4.381 .000 c.m/s

27 HYDROGRAPH DISPLAY
 5 is # of Hyeto/Hydrograph chosen
 Volume = .2307839E+05 c.m

20 MANUAL

Stormwater Management Plan

Rosedale Subdivision – City of Port Colborne

Development Conditions without SWM

```

Output File (4.7) NOSWM.OUT      opened 2023-09-21  9:54
Units used are defined by G =    9.810
24 144 10.000 are MAXDT MAXHYD & DTMIN values
Licensee: UPPER CANADA CONSULTANTS
35 COMMENT
4 1 line(s) of comment
ROSEDALE SUBDIVISION
STORMWATER MANAGEMENT PLAN
FUTURE CONDITIONS TO BIEDERMAN DRAIN
OCTOBER 2022
14 START
1 1=Zero; 2=Define
35 COMMENT
3 1 line(s) of comment
*****
* MTO 2 YEAR DESIGN STORM EVENT *
*****
2 STORM
1 1=Chicago;2=Huff;3=User;4=Cdnlhr;5=Historic
397.149 Coefficient a
.000 Constant b (min)
.699 Exponent c
.450 Fraction to peak r
240.000 Duration ó 240 min
34.451 mm Total depth
3 IMPERVIOUS
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.015 Manning "n"
98.000 SCS Curve No or C
.100 Ia/S Coefficient
.518 Initial Abstraction
35 COMMENT
1 1 line(s) of comment
*** FIELD - DRAINAGE AREA FX ***
4 CATCHMENT
1.000 ID No.ó 99999
3.440 Area in hectares
150.000 Length (PERV) metres
1.000 Gradient (%)
.500 Per cent Impervious
150.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.023 .000 .000 .000 c.m/s
.204 .841 .207 C perv/imperv/total
15 ADD RUNOFF
.023 .023 .000 .000 c.m/s
11 CHANNEL
.300 Base Width =
3.000 Left bank slope 1:
3.000 Right bank slope 1:
.030 Manning's "n"
.500 O/a Depth in metres
1.000 Select Grade in %
Depth = .084 metres
Velocity = .488 m/sec
Flow Capacity = 1.222 c.m/s
Critical depth = .067 metres
9 ROUTE
400.000 Conduit Length
.489 Supply X-factor <.5
307.501 Supply K-lag (sec)
.500 Beta weighting factor
600.000 Routing timestep
2 No. of sub-reaches
.023 .023 .023 .000 c.m/s
16 NEXT LINK
.023 .023 .023 .000 c.m/s
35 COMMENT
1 1 line(s) of comment
*** EXISTING RESIDENTIAL - DRAINAGE AREA WT ***
4 CATCHMENT
1.000 ID No.ó 99999
10.840 Area in hectares
300.000 Length (PERV) metres
1.000 Gradient (%)
25.000 Per cent Impervious
300.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.367 .023 .023 .000 c.m/s
.204 .849 .365 C perv/imperv/total
15 ADD RUNOFF
.367 .370 .023 .000 c.m/s
11 CHANNEL
.300 Base Width =
3.000 Left bank slope 1:
3.000 Right bank slope 1:
.030 Manning's "n"
.500 O/a Depth in metres
1.000 Select Grade in %
Depth = .304 metres
Velocity = 1.006 m/sec
Flow Capacity = 1.222 c.m/s
Critical depth = .270 metres
9 ROUTE
200.000 Conduit Length
.468 Supply X-factor <.5
149.160 Supply K-lag (sec)
.500 Beta weighting factor
150.000 Routing timestep
1 No. of sub-reaches
.367 .370 .325 .000 c.m/s
16 NEXT LINK
.367 .325 .325 .000 c.m/s
35 COMMENT
1 1 line(s) of comment
*** MEADOW HEIGHTS - DRAINAGE AREA MH ***
4 CATCHMENT
1.000 ID No.ó 99999
29.250 Area in hectares
500.000 Length (PERV) metres
2.000 Gradient (%)
35.700 Per cent Impervious
500.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
1.385 .325 .325 .000 c.m/s
.204 .841 .431 C perv/imperv/total
15 ADD RUNOFF
1.385 1.710 .325 .000 c.m/s
27 HYDROGRAPH DISPLAY
5 is # of Hyeto/Hydrograph chosen
Volume = .5951399E+04 c.m
8 PIPE
.500 Minimum velocity m/sec
2.920 Maximum velocity m/sec
.013 Pipe Manning's 'n'
1.350 Diameter in metres
.600 Select Grade in %
Depth = .605 metres
Velocity = 2.750 m/sec
Pipe Capacity = 4.134 c.m/s
Critical depth= .692 metres
9 ROUTE
500.000 Conduit Length
.442 Supply X-factor <.5
136.363 Supply K-lag (sec)
.500 Beta weighting factor
150.000 Routing timestep
1 No. of sub-reaches
1.385 1.710 1.493 .000 c.m/s
16 NEXT LINK
1.385 1.493 1.493 .000 c.m/s
35 COMMENT
1 1 line(s) of comment
*** ROSEDALE - DRAINAGE AREA FUT ***
4 CATCHMENT
1.000 ID No.ó 99999
12.770 Area in hectares
400.000 Length (PERV) metres
3.000 Gradient (%)
70.000 Per cent Impervious
400.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
1.204 1.493 1.493 .000 c.m/s
.204 .852 .657 C perv/imperv/total
15 ADD RUNOFF
1.204 2.697 1.493 .000 c.m/s
27 HYDROGRAPH DISPLAY
5 is # of Hyeto/Hydrograph chosen
Volume = .8842857E+04 c.m
14 START
1 1=Zero; 2=Define
35 COMMENT
3 1 line(s) of comment
*****
* MTO 5 YEAR DESIGN STORM EVENT *
*****
2 STORM
1 1=Chicago;2=Huff;3=User;4=Cdnlhr;5=Historic
524.867 Coefficient a
.000 Constant b (min)
.699 Exponent c
.450 Fraction to peak r
240.000 Duration ó 240 min
45.530 mm Total depth
3 IMPERVIOUS
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.015 Manning "n"
98.000 SCS Curve No or C
.100 Ia/S Coefficient
.518 Initial Abstraction
35 COMMENT
1 1 line(s) of comment
*** FIELD - DRAINAGE AREA FX ***
4 CATCHMENT
1.000 ID No.ó 99999
3.440 Area in hectares
150.000 Length (PERV) metres
1.000 Gradient (%)
.500 Per cent Impervious
150.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.055 .000 1.493 .000 c.m/s
.278 .859 .280 C perv/imperv/total
15 ADD RUNOFF
.055 .055 1.493 .000 c.m/s
11 CHANNEL
.300 Base Width =
3.000 Left bank slope 1:
3.000 Right bank slope 1:
.030 Manning's "n"
.500 O/a Depth in metres

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Stormwater Management Plan

Rosedale Subdivision – City of Port Colborne

```

1.000 Select Grade in %
Depth = .129 metres
Velocity = .616 m/sec
Flow Capacity = 1.222 c.m/s
Critical depth = .106 metres
9 ROUTE
400.000 Conduit Length
.492 Supply X-factor <.5
487.040 Supply K-lag (sec)
.500 Beta weighting factor
300.000 Routing timestep
1 No. of sub-reaches
.055 .055 .053 .000 c.m/s
16 NEXT LINK
.055 .053 .053 .000 c.m/s
35 COMMENT
1 line(s) of comment
*** EXISTING RESIDENTIAL - DRAINAGE AREA WT ***
4 CATCHMENT
1.000 ID No.6 99999
10.840 Area in hectares
300.000 Length (PERV) metres
1.000 Gradient (%)
25.000 Per cent Impervious
300.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.515 .053 .053 .000 c.m/s
.278 .884 .429 C perv/imperv/total
15 ADD RUNOFF
.515 .525 .053 .000 c.m/s
11 CHANNEL
.300 Base Width =
3.000 Left bank slope 1:
3.000 Right bank slope 1:
.030 Manning's "n"
.500 O/a Depth in metres
1.000 Select Grade in %
Depth = .352 metres
Velocity = 1.098 m/sec
Flow Capacity = 1.222 c.m/s
Critical depth = .317 metres
9 ROUTE
200.000 Conduit Length
.463 Supply X-factor <.5
136.564 Supply K-lag (sec)
.500 Beta weighting factor
120.000 Routing timestep
1 No. of sub-reaches
.515 .525 .476 .000 c.m/s
16 NEXT LINK
.515 .476 .476 .000 c.m/s
35 COMMENT
1 line(s) of comment
*** MEADOW HEIGHTS - DRAINAGE AREA MH ***
4 CATCHMENT
1.000 ID No.6 99999
29.250 Area in hectares
500.000 Length (PERV) metres
2.000 Gradient (%)
35.700 Per cent Impervious
500.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
1.941 .476 .476 .000 c.m/s
.278 .882 .493 C perv/imperv/total
15 ADD RUNOFF
1.941 2.416 .476 .000 c.m/s
27 HYDROGRAPH DISPLAY
5 is # of Hyeto/Hydrograph chosen
Volume = .9127035E+04 c.m
8 PIPE
.500 Minimum velocity m/sec
2.920 Maximum velocity m/sec
.013 Pipe Manning's 'n'
1.350 Diameter in metres
.600 Select Grade in %
Depth = .741 metres
Velocity = 3.000 m/sec
Pipe Capacity = 4.134 c.m/s
Critical depth = .829 metres
9 ROUTE
500.000 Conduit Length
.424 Supply X-factor <.5
124.986 Supply K-lag (sec)
.500 Beta weighting factor
120.000 Routing timestep
1 No. of sub-reaches
1.941 2.416 2.180 .000 c.m/s
16 NEXT LINK
1.941 2.180 2.180 .000 c.m/s
35 COMMENT
1 line(s) of comment
*** ROSEDALE - DRAINAGE AREA RD ***
4 CATCHMENT
1.000 ID No.6 99999
12.770 Area in hectares
400.000 Length (PERV) metres
2.000 Gradient (%)
70.000 Per cent Impervious
400.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
1.643 2.180 2.180 .000 c.m/s
.278 .883 .702 C perv/imperv/total
15 ADD RUNOFF
1.643 3.822 2.180 .000 c.m/s
27 HYDROGRAPH DISPLAY
5 is # of Hyeto/Hydrograph chosen
Volume = .1320661E+05 c.m
START
1 1=Zero; 2=Define
35 COMMENT
3 line(s) of comment
*****
* MTO 10 YEAR DESIGN STORM EVENT *
*****
2 STORM
1 1=Chicago;2=Huff;3=User;4=Cdnlhr;5=Historic
608.845 Coefficient a
.000 Constant b (min)
.699 Exponent c
.450 Fraction to peak r
240.000 Duration 6 240 min
52.815 mm Total depth
3 IMPERVIOUS
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.015 Manning "n"
98.000 SCS Curve No or C
.100 Ia/S Coefficient
.518 Initial Abstraction
35 COMMENT
1 line(s) of comment
*** FIELD - DRAINAGE AREA FX ***
4 CATCHMENT
1.000 ID No.6 99999
3.440 Area in hectares
150.000 Length (PERV) metres
1.000 Gradient (%)
.500 Per cent Impervious
150.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.079 .000 2.180 .000 c.m/s
.320 .878 .322 C perv/imperv/total
15 ADD RUNOFF
.079 .079 2.180 .000 c.m/s
11 CHANNEL
.300 Base Width =
3.000 Left bank slope 1:
3.000 Right bank slope 1:
.030 Manning's "n"
.500 O/a Depth in metres
1.000 Select Grade in %
Depth = .154 metres
Velocity = .679 m/sec
Flow Capacity = 1.222 c.m/s
Critical depth = .129 metres
9 ROUTE
400.000 Conduit Length
.491 Supply X-factor <.5
441.992 Supply K-lag (sec)
.500 Beta weighting factor
300.000 Routing timestep
1 No. of sub-reaches
.079 .079 .077 .000 c.m/s
16 NEXT LINK
.079 .077 .077 .000 c.m/s
35 COMMENT
1 line(s) of comment
*** EXISTING RESIDENTIAL - DRAINAGE AREA WT ***
4 CATCHMENT
1.000 ID No.6 99999
10.840 Area in hectares
300.000 Length (PERV) metres
1.000 Gradient (%)
25.000 Per cent Impervious
300.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.613 .077 .077 .000 c.m/s
.320 .897 .464 C perv/imperv/total
15 ADD RUNOFF
.613 .632 .077 .000 c.m/s
11 CHANNEL
.300 Base Width =
3.000 Left bank slope 1:
3.000 Right bank slope 1:
.030 Manning's "n"
.500 O/a Depth in metres
1.000 Select Grade in %
Depth = .381 metres
Velocity = 1.150 m/sec
Flow Capacity = 1.222 c.m/s
Critical depth = .344 metres
9 ROUTE
200.000 Conduit Length
.460 Supply X-factor <.5
130.387 Supply K-lag (sec)
.500 Beta weighting factor
120.000 Routing timestep
1 No. of sub-reaches
.613 .632 .579 .000 c.m/s
16 NEXT LINK
.613 .579 .579 .000 c.m/s
35 COMMENT
1 line(s) of comment
*** MEADOW HEIGHTS - DRAINAGE AREA MH ***
4 CATCHMENT

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Stormwater Management Plan

Rosedale Subdivision – City of Port Colborne

1.000	ID No.6 99999	9	ROUTE
29.250	Area in hectares	400.000	Conduit Length
500.000	Length (PERV) metres	.489	Supply X-factor <.5
2.000	Gradient (%)	391.534	Supply K-lag (sec)
35.700	Per cent Impervious	.500	Beta weighting factor
500.000	Length (IMPERV)	300.000	Routing timestep
.000	%Imp. with Zero Dpth	1	No. of sub-reaches
1	Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat	.127	.127
.250	Manning "n"	.122	.000 c.m/s
77.000	SCS Curve No or C	16	NEXT LINK
.100	Ia/S Coefficient	.127	.122
7.587	Initial Abstraction	.122	.000 c.m/s
1	Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv	35	COMMENT
2.305	.579	.579	1 line(s) of comment
.320	.898	.526	*** EXISTING RESIDENTIAL - DRAINAGE AREA WT ***
			4
15	ADD RUNOFF		CATCHMENT
2.305	2.884	.579	1.000 ID No.6 99999
			10.840 Area in hectares
27	HYDROGRAPH DISPLAY		300.000 Length (PERV) metres
5	is # of Hyeto/Hydrograph chosen		1.000 Gradient (%)
Volume =	.1136950E+05 c.m		25.000 Per cent Impervious
8	PIPE		300.000 Length (IMPERV)
.500	Minimum velocity m/sec		.000 %Imp. with Zero Dpth
2.920	Maximum velocity m/sec		1
.013	Pipe Manning's 'n'		Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
1.350	Diameter in metres		.250 Manning "n"
.600	Select Grade in %		77.000 SCS Curve No or C
Depth =	.830 metres		.100 Ia/S Coefficient
Velocity =	3.123 m/sec		7.587 Initial Abstraction
Pipe Capacity =	4.134 c.m/s		1
Critical depth =	.908 metres		Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
9	ROUTE		.742 .122 .122 .000 c.m/s
500.000	Conduit Length		.367 .911 .503 C perv/imperv/total
.407	Supply X-factor <.5		15
120.096	Supply K-lag (sec)		ADD RUNOFF
.500	Beta weighting factor		.742 .775 .122 .000 c.m/s
120.000	Routing timestep		11
1	No. of sub-reaches		CHANNEL
2.305	2.884	2.637	.300 Base Width =
16	NEXT LINK	2.637	3.000 Left bank slope 1:
2.305	2.637	2.637	3.000 Right bank slope 1:
35	COMMENT		.030 Manning's "n"
1	line(s) of comment		.500 O/a Depth in metres
*** ROSEDALE - DRAINAGE AREA FUT ***			Select Grade in %
4	CATCHMENT		1.000
1.000	ID No.6 99999		Depth =
12.770	Area in hectares		415 metres
400.000	Length (PERV) metres		Velocity =
3.000	Gradient (%)		1.211 m/sec
70.000	Per cent Impervious		Flow Capacity =
400.000	Length (IMPERV)		1.222 c.m/s
.000	%Imp. with Zero Dpth		Critical depth =
.000	%Imp. with Zero Dpth		.377 metres
1	Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat		9
.250	Manning "n"		ROUTE
77.000	SCS Curve No or C		200.000 Conduit Length
.100	Ia/S Coefficient		.457 Supply X-factor <.5
7.587	Initial Abstraction		123.848 Supply K-lag (sec)
1	Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv		.500 Beta weighting factor
1.861	2.637	2.637	120.000 Routing timestep
.320	.893	.721	1
			No. of sub-reaches
15	ADD RUNOFF		.742 .775 .720 .000 c.m/s
1.861	4.498	2.637	16
			NEXT LINK
27	HYDROGRAPH DISPLAY		.742 .720 .720 .000 c.m/s
5	is # of Hyeto/Hydrograph chosen		35
Volume =	.1623196E+05 c.m		COMMENT
14	START		1
1	l=Zero; 2=Define		line(s) of comment
35	COMMENT		*** MEADOW HEIGHTS - DRAINAGE AREA MH ***
3	line(s) of comment		4
*****			CATCHMENT
* MTO 25 YEAR DESIGN STORM EVENT *			1.000 ID No.6 99999
*****			29.250 Area in hectares
2	STORM		500.000 Length (PERV) metres
1	l=Chicago; 2=Huff; 3=User; 4=Cdnlhr; 5=Historic		2.000 Gradient (%)
715.568	Coefficient a		35.700 Per cent Impervious
.000	Constant b (min)		500.000 Length (IMPERV)
.699	Exponent c		.000 %Imp. with Zero Dpth
.450	Fraction to peak r		1
240.000	Duration 6 240 min		Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
	62.073 mm Total depth		.250 Manning "n"
3	IMPERVIOUS		77.000 SCS Curve No or C
1	Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat		.100 Ia/S Coefficient
.015	Manning "n"		7.587 Initial Abstraction
98.000	SCS Curve No or C		1
.100	Ia/S Coefficient		Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.518	Initial Abstraction		.127 .000 2.637 .000 c.m/s
35	COMMENT		.367 .898 .369 C perv/imperv/total
1	line(s) of comment		15
*** FIELD - DRAINAGE AREA FX ***			ADD RUNOFF
4	CATCHMENT		.127 .127 2.637 .000 c.m/s
1.000	ID No.6 99999		11
3.440	Area in hectares		CHANNEL
150.000	Length (PERV) metres		.300 Base Width =
1.000	Gradient (%)		3.000 Left bank slope 1:
.500	Per cent Impervious		3.000 Right bank slope 1:
150.000	Length (IMPERV)		.030 Manning's "n"
.000	%Imp. with Zero Dpth		.500 O/a Depth in metres
.000	%Imp. with Zero Dpth		1.000 Select Grade in %
1	Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat		Depth =
.250	Manning "n"		.190 metres
77.000	SCS Curve No or C		Velocity =
.100	Ia/S Coefficient		.766 m/sec
7.587	Initial Abstraction		Pipe Capacity =
1	Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv		1.222 c.m/s
.127	.000	2.637	Critical depth =
.367	.898	.369	.162 metres
15	ADD RUNOFF		
.127	.127	2.637	
11	CHANNEL		
.300	Base Width =		
3.000	Left bank slope 1:		
3.000	Right bank slope 1:		
.030	Manning's "n"		
.500	O/a Depth in metres		
1.000	Select Grade in %		
Depth =	.190 metres		
Velocity =	.766 m/sec		
Pipe Capacity =	1.222 c.m/s		
Critical depth =	.162 metres		
9	ROUTE		
500.000	Conduit Length		
.377	Supply X-factor <.5		
115.797	Supply K-lag (sec)		
.500	Beta weighting factor		
120.000	Routing timestep		
1	No. of sub-reaches		
2.767	3.486	3.226	
16	NEXT LINK	3.226	
2.767	3.226	3.226	
35	COMMENT		
1	line(s) of comment		
*** ROSEDALE - DRAINAGE AREA FUT ***			
4	CATCHMENT		
1.000	ID No.6 99999		
12.770	Area in hectares		
400.000	Length (PERV) metres		
3.000	Gradient (%)		
70.000	Per cent Impervious		
400.000	Length (IMPERV)		
.000	%Imp. with Zero Dpth		
1	Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat		
.250	Manning "n"		
77.000	SCS Curve No or C		
.100	Ia/S Coefficient		
7.587	Initial Abstraction		
1	Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv		
2.199	3.226	3.226	
.367	.901	.740	
15	ADD RUNOFF		
2.199	5.425	3.226	

Stormwater Management Plan

Rosedale Subdivision – City of Port Colborne

27	HYDROGRAPH DISPLAY	500.000	Length (IMPERV)	
5	is # of Hyeto/Hydrograph chosen	.000	%Imp. with Zero Dpth	
	Volume = .2022603E+05 c.m	1	Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat	
14	START	.250	Manning "n"	
1	1=Zero; 2=Define	77.000	SCS Curve No or C	
35	COMMENT	.100	Ia/S Coefficient	
3	line(s) of comment	7.587	Initial Abstraction	
	*****	1	Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv	
	* MTO 50 YEAR DESIGN STORM EVENT *	3.111	.829	.000 c.m/s
	*****	.397	.919	.584 C perv/imperv/total
2	STORM	15	ADD RUNOFF	
1	1=Chicago;2=Huff;3=User;4=Cdnlhr;5=Historic	3.111	3.940	.829 .000 c.m/s
794.298	Coefficient a	27	HYDROGRAPH DISPLAY	
.000	Constant b (min)	5	is # of Hyeto/Hydrograph chosen	
.699	Exponent c		Volume = .1664438E+05 c.m	
.450	Fraction to peak r	8	PIPE	
240.000	Duration δ 240 min	.500	Minimum velocity m/sec	
68.903 mm	Total depth	2.920	Maximum velocity m/sec	
3	IMPERVIOUS	.013	Pipe Manning's 'n'	
1	Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat	1.350	Diameter in metres	
.015	Manning "n"	.600	Select Grade in %	
98.000	SCS Curve No or C		Depth = 1.053 metres	
.100	Ia/S Coefficient		Velocity = 3.288 m/sec	
.518	Initial Abstraction		Pipe Capacity = 4.134 c.m/s	
35	COMMENT		Critical depth= 1.060 metres	
1	line(s) of comment	9	ROUTE	
*** FIELD - DRAINAGE AREA FX ***		500.000	Conduit Length	
4	CATCHMENT	.344	Supply X-factor <.5	
1.000	ID No.6 99999	114.065	Supply K-lag (sec)	
3.440	Area in hectares	.500	Beta weighting factor	
150.000	Length (PERV) metres	120.000	Routing timestep	
1.000	Gradient (%)	1	No. of sub-reaches	
.500	Per cent Impervious	3.111	3.940	3.669 .000 c.m/s
150.000	Length (IMPERV)	16	NEXT LINK	
.000	%Imp. with Zero Dpth	3.111	3.669	3.669 .000 c.m/s
1	Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat	35	COMMENT	
.250	Manning "n"	1	line(s) of comment	
77.000	SCS Curve No or C	*** ROSEDALE - DRAINAGE AREA FUT ***		
.100	Ia/S Coefficient	4	CATCHMENT	
7.587	Initial Abstraction	1.000	ID No.6 99999	
1	Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv	12.770	Area in hectares	
.161	.000	400.000	Length (PERV) metres	
.397	.909	3.000	Gradient (%)	
15	ADD RUNOFF	70.000	Per cent Impervious	
.161	.161	400.000	Length (IMPERV)	
11	CHANNEL	.000	%Imp. with Zero Dpth	
.300	Base Width =	1	Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat	
3.000	Left bank slope 1:	.250	Manning "n"	
3.000	Right bank slope 1:	77.000	SCS Curve No or C	
.030	Manning's "n"	.100	Ia/S Coefficient	
.500	O/a Depth in metres	7.587	Initial Abstraction	
1.000	Select Grade in %	1	Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv	
Depth = .211 metres		2.448	3.669	3.669 .000 c.m/s
Velocity = .814 m/sec		.398	.903	.752 C perv/imperv/total
Flow Capacity = 1.222 c.m/s		15	ADD RUNOFF	
Critical depth = .182 metres		27	HYDROGRAPH DISPLAY	
9	ROUTE	5	is # of Hyeto/Hydrograph chosen	
400.000	Conduit Length		Volume = .2325709E+05 c.m	
.488	Supply X-factor <.5	14	START	
368.744	Supply K-lag (sec)	1	1=Zero; 2=Define	
.500	Beta weighting factor	35	COMMENT	
300.000	Routing timestep	3	line(s) of comment	
1	No. of sub-reaches	*****		
.161	.161	* MTO 100 YEAR DESIGN STORM EVENT *		
16	NEXT LINK	*****		
.161	.154	2	STORM	
35	COMMENT	1	1=Chicago;2=Huff;3=User;4=Cdnlhr;5=Historic	
1	line(s) of comment	871.279	Coefficient a	
*** EXISTING RESIDENTIAL - DRAINAGE AREA WT ***		.000	Constant b (min)	
4	CATCHMENT	.699	Exponent c	
1.000	ID No.6 99999	.450	Fraction to peak r	
10.840	Area in hectares	240.000	Duration δ 240 min	
300.000	Length (PERV) metres		75.581 mm	Total depth
1.000	Gradient (%)	3	IMPERVIOUS	
25.000	Per cent Impervious	1	Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat	
300.000	Length (IMPERV)	.015	Manning "n"	
.000	%Imp. with Zero Dpth	98.000	SCS Curve No or C	
1	Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat	.100	Ia/S Coefficient	
.250	Manning "n"	.518	Initial Abstraction	
77.000	SCS Curve No or C	35	COMMENT	
.100	Ia/S Coefficient	1	line(s) of comment	
7.587	Initial Abstraction	*** FIELD - DRAINAGE AREA FX ***		
1	Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv	4	CATCHMENT	
.841	.154	1.000	ID No.6 99999	
.397	.917	3.440	Area in hectares	
15	ADD RUNOFF	150.000	Length (PERV) metres	
.841	.888	1.000	Gradient (%)	
11	CHANNEL	.500	Per cent Impervious	
.300	Base Width =	150.000	Length (IMPERV)	
3.000	Left bank slope 1:	.000	%Imp. with Zero Dpth	
3.000	Right bank slope 1:	1	Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat	
.030	Manning's "n"	.250	Manning "n"	
.500	O/a Depth in metres	77.000	SCS Curve No or C	
1.000	Select Grade in %	.100	Ia/S Coefficient	
Depth = .439 metres		7.587	Initial Abstraction	
Velocity = 1.253 m/sec		1	Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv	
Flow Capacity = 1.222 c.m/s		.196	.000	3.669 .000 c.m/s
Critical depth = .400 metres		.425	.917	.427 C perv/imperv/total
9	ROUTE	15	ADD RUNOFF	
200.000	Conduit Length	11	CHANNEL	
.455	Supply X-factor <.5	.300	Base Width =	
119.694	Supply K-lag (sec)	3.000	Left bank slope 1:	
.500	Beta weighting factor	3.000	Right bank slope 1:	
120.000	Routing timestep	.030	Manning's "n"	
1	No. of sub-reaches	.500	O/a Depth in metres	
.841	.888	1.000	Select Grade in %	
16	NEXT LINK	Depth = .231 metres		
.841	.829	Velocity = .856 m/sec		
35	COMMENT	Flow Capacity = 1.222 c.m/s		
1	line(s) of comment	Critical depth = .200 metres		
*** MEADOW HEIGHTS - DRAINAGE AREA MH ***		9	ROUTE	
4	CATCHMENT	400.000	Conduit Length	
1.000	ID No.6 99999	.487	Supply X-factor <.5	
29.250	Area in hectares	350.564	Supply K-lag (sec)	
500.000	Length (PERV) metres	.500	Beta weighting factor	
2.000	Gradient (%)			
35.700	Per cent Impervious			

Stormwater Management Plan

Rosedale Subdivision – City of Port Colborne

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300.000 Routing timestep
1 No. of sub-reaches
.196 .196 .186 .000 c.m/s
16 NEXT LINK .196 .186 .186 .000 c.m/s
35 COMMENT
1 line(s) of comment
*** EXISTING RESIDENTIAL - DRAINAGE AREA WT ***
4 CATCHMENT
1.000 ID No.6 99999
10.840 Area in hectares
300.000 Length (PERV) metres
1.000 Gradient (%)
25.000 Per cent Impervious
300.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.924 .186 .186 .000 c.m/s
.425 .922 .549 C perv/imperv/total
15 ADD RUNOFF .924 .988 .186 .000 c.m/s
11 CHANNEL
.300 Base Width =
3.000 Left bank slope 1:
3.000 Right bank slope 1:
.030 Manning's "n"
.500 O/a Depth in metres
1.000 Select Grade in %
Depth = .458 metres
Velocity = 1.287 m/sec
Flow Capacity = 1.222 c.m/s
Critical depth = .420 metres
9 ROUTE
200.000 Conduit Length
.453 Supply X-factor <.5
116.540 Supply K-lag (sec)
.500 Beta weighting factor
120.000 Routing timestep
1 No. of sub-reaches
.924 .988 .929 .000 c.m/s
16 NEXT LINK .924 .929 .929 .000 c.m/s
35 COMMENT
1 line(s) of comment
*** MEADOW HEIGHTS - DRAINAGE AREA MH ***
4 CATCHMENT
1.000 ID No.6 99999
29.250 Area in hectares
500.000 Length (PERV) metres
2.000 Gradient (%)
35.700 Per cent Impervious
500.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
3.453 .929 .929 .000 c.m/s
.425 .926 .604 C perv/imperv/total
15 ADD RUNOFF 3.453 4.381 .929 .000 c.m/s
27 HYDROGRAPH DISPLAY
5 is # of Hyeto/Hydrograph chosen
Volume = .1895466E+05 c.m
8 PIPE
.500 Minimum velocity m/sec
2.920 Maximum velocity m/sec
.013 Pipe Manning's "n"
1.350 Diameter in metres
.600 Select Grade in %
Surcharged HGL= .674 %
Velocity = 3.061 m/sec
Pipe Capacity = 4.134 c.m/s
Critical depth= 1.113 metres
9 ROUTE
500.000 Conduit Length
.500 Supply X-factor <.5
.000 Supply K-lag (sec)
.500 Beta weighting factor
600.000 Routing timestep
1 No. of sub-reaches
3.453 4.381 4.381 .000 c.m/s
16 NEXT LINK 3.453 4.381 4.381 .000 c.m/s
35 COMMENT
1 line(s) of comment
*** ROSEDALE - DRAINAGE AREA FUT ***
4 CATCHMENT
1.000 ID No.6 99999
12.770 Area in hectares
400.000 Length (PERV) metres
3.000 Gradient (%)
70.000 Per cent Impervious
400.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
2.688 4.381 4.381 .000 c.m/s
.425 .904 .760 C perv/imperv/total
15 ADD RUNOFF 2.688 7.069 4.381 .000 c.m/s
27 HYDROGRAPH DISPLAY
5 is # of Hyeto/Hydrograph chosen
Volume = .2629441E+05 c.m
20 MANUAL

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Stormwater Management Plan

Rosedale Subdivision – City of Port Colborne

Development Conditions with SWM

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Output File (4.7) SWM.OUT      opened 2023-10-06 13:45
Units used are defined by G = 9.810
24 144 10.000 are MAXDT MAXHYD & DTMIN values
Licensee: UPPER CANADA CONSULTANTS
35 COMMENT
4 line(s) of comment
ROSEDALE SUBDIVISION
STORMWATER MANAGEMENT PLAN
FUTURE CONDITIONS TO BIEDERMAN DRAIN
OCTOBER 2022
14 START
1 1=Zero; 2=Define
35 COMMENT
3 line(s) of comment
*****
* 25MM DESIGN STORM EVENT *
*****
2 STORM
1 1=Chicago;2=Huff;3=User;4=Cdnlhr;5=Historic
512.000 Coefficient a
6.000 Constant b (min)
.800 Exponent c
.450 Fraction to peak r
240.000 Duration  $\delta$  240 min
25.035 mm Total depth
3 IMPERVIOUS
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.015 Manning "n"
98.000 SCS Curve No or C
.100 Ia/S Coefficient
.518 Initial Abstraction
4 CATCHMENT
1.000 ID No.  $\delta$  99999
12.770 Area in hectares
400.000 Length (PERV) metres
2.000 Gradient (%)
70.000 Per cent Impervious
400.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglrr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.821 .000 .000 .000 c.m/s
.130 .799 .598 C perv/imperv/total
15 ADD RUNOFF
.821 .821 .000 .000 c.m/s
27 HYDROGRAPH DISPLAY
5 is # of Hyeto/Hydrograph chosen
Volume = .1907682E+04 c.m
10 POND
9 Depth - Discharge - Volume sets
174.850 .000 .0
175.350 .0310 1713.0
175.600 .0400 2746.0
175.760 .0800 3467.0
175.850 .0829 3893.0
176.350 .0830 6538.0
176.650 .0831 8354.0
176.750 .233 8999.0
176.850 .473 9663.0
Peak Outflow = .028 c.m/s
Maximum Depth = 175.306 metres
Maximum Storage = 1562. c.m
.821 .821 .028 .000 c.m/s
14 START
1 1=Zero; 2=Define
35 COMMENT
3 line(s) of comment
*****
* MTO 2 YEAR DESIGN STORM EVENT *
*****
2 STORM
1 1=Chicago;2=Huff;3=User;4=Cdnlhr;5=Historic
397.149 Coefficient a
.000 Constant b (min)
.699 Exponent c
.450 Fraction to peak r
240.000 Duration  $\delta$  240 min
34.451 mm Total depth
3 IMPERVIOUS
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.015 Manning "n"
98.000 SCS Curve No or C
.100 Ia/S Coefficient
.518 Initial Abstraction
35 COMMENT
1 line(s) of comment
*** FIELD - DRAINAGE AREA FX ***
4 CATCHMENT
1.000 ID No.  $\delta$  99999
3.440 Area in hectares
150.000 Length (PERV) metres
1.000 Gradient (%)
.500 Per cent Impervious
150.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
.1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglrr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.023 .000 .028 .000 c.m/s
.204 .841 .207 C perv/imperv/total
15 ADD RUNOFF
.023 .023 .028 .000 c.m/s
11 CHANNEL
.300 Base Width =
3.000 Left bank slope 1:
3.000 Right bank slope 1:
.030 Manning's "n"
.500 O/a Depth in metres
1.000 Select Grade in %
Depth = .084 metres
Velocity = .488 m/sec
Flow Capacity = 1.222 c.m/s
Critical depth = .067 metres
ROUTE
400.000 Conduit Length
.489 Supply X-factor <.5
307.501 Supply K-lag (sec)
.500 Beta weighting factor
600.000 Routing timestep
2 No. of sub-reaches
.023 .023 .023 .000 c.m/s
16 NEXT LINK
.023 .023 .023 .000 c.m/s
35 COMMENT
1 line(s) of comment
*** EXISTING RESIDENTIAL - DRAINAGE AREA WT ***
4 CATCHMENT
1.000 ID No.  $\delta$  99999
10.840 Area in hectares
300.000 Length (PERV) metres
1.000 Gradient (%)
25.000 Per cent Impervious
300.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglrr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.367 .023 .023 .000 c.m/s
.204 .849 .365 C perv/imperv/total
15 ADD RUNOFF
.367 .370 .023 .000 c.m/s
11 CHANNEL
.300 Base Width =
3.000 Left bank slope 1:
3.000 Right bank slope 1:
.030 Manning's "n"
.500 O/a Depth in metres
1.000 Select Grade in %
Depth = .304 metres
Velocity = 1.006 m/sec
Flow Capacity = 1.222 c.m/s
Critical depth = .270 metres
ROUTE
200.000 Conduit Length
.468 Supply X-factor <.5
149.160 Supply K-lag (sec)
.500 Beta weighting factor
150.000 Routing timestep
1 No. of sub-reaches
.367 .370 .325 .000 c.m/s
16 NEXT LINK
.367 .325 .325 .000 c.m/s
35 COMMENT
1 line(s) of comment
*** MEADOW HEIGHTS - DRAINAGE AREA MH ***
4 CATCHMENT
1.000 ID No.  $\delta$  99999
29.250 Area in hectares
500.000 Length (PERV) metres
2.000 Gradient (%)
35.700 Per cent Impervious
500.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglrr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
1.385 .325 .325 .000 c.m/s
.204 .841 .431 C perv/imperv/total
15 ADD RUNOFF
1.385 1.710 .325 .000 c.m/s
27 HYDROGRAPH DISPLAY
5 is # of Hyeto/Hydrograph chosen
Volume = .5951403E+04 c.m
8 PIPE
.500 Minimum velocity m/sec
2.920 Maximum velocity m/sec
.013 Pipe Manning's 'n'
1.350 Diameter in metres
.600 Select Grade in %
Depth = .605 metres
Velocity = 2.750 m/sec
Pipe Capacity = 4.134 c.m/s
Critical depth= .692 metres
ROUTE
500.000 Conduit Length
.442 Supply X-factor <.5
136.363 Supply K-lag (sec)
.500 Beta weighting factor
150.000 Routing timestep
1 No. of sub-reaches
1.385 1.710 1.493 .000 c.m/s
17 COMBINE
1 Junction Node No.
1.385 1.710 1.493 1.493 c.m/s
14 START
1 1=Zero; 2=Define
35 COMMENT
1 line(s) of comment
*** ROSEDALE - DRAINAGE AREA FUT ***
4 CATCHMENT
1.000 ID No.  $\delta$  99999
14.230 Area in hectares
400.000 Length (PERV) metres
3.000 Gradient (%)
70.000 Per cent Impervious
400.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat

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Stormwater Management Plan

Rosedale Subdivision – City of Port Colborne

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.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
1.342 .000 1.493 1.493 c.m/s
.204 .852 .657 C perv/imperv/total
15 ADD RUNOFF 1.342 1.342 1.493 1.493 c.m/s
27 HYDROGRAPH DISPLAY
5 is # of Hyeto/Hydrograph chosen
Volume = .3222296E+04 c.m
35 COMMENT
1 line(s) of comment
*** SITE - EX FLOWS OF 63 L/S DURING 2 YR ***
10 POND
9 Depth - Discharge - Volume sets
174.850 .000 .0
175.350 .0310 1713.0
175.600 .0400 2746.0
175.760 .0800 3467.0
175.850 .0829 3893.0
176.350 .0830 6538.0
176.650 .0831 8354.0
176.750 .233 8999.0
176.850 .473 9663.0
Peak Outflow = .040 c.m/s
Maximum Depth = 175.591 metres
Maximum Storage = 2711. c.m
1.342 1.342 .040 1.493 c.m/s
17 COMBINE
1 Junction Node No.
1.342 1.342 .040 1.512 c.m/s
35 COMMENT
1 line(s) of comment
*** OVERALL - EX FLOWS OF 1512 L/S DURING 2 YR ***
18 CONFLUENCE
1 Junction Node No.
1.342 1.512 .040 .000 c.m/s
14 START
1 l=Zero; 2=Define
35 COMMENT
3 line(s) of comment
*****
* MTO 5 YEAR DESIGN STORM EVENT *
*****
2 STORM
1 l=Chicago;2=Huff;3=User;4=Cdnlhr;5=Historic
524.867 Coefficient a
.000 Constant b (min)
.699 Exponent c
.450 Fraction to peak r
240.000 Duration o 240 min
45.530 mm Total depth
3 IMPERVIOUS
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.015 Manning "n"
98.000 SCS Curve No or C
.100 Ia/S Coefficient
.518 Initial Abstraction
35 COMMENT
1 line(s) of comment
*** FIELD - DRAINAGE AREA FX ***
4 CATCHMENT
1.000 ID No.6 99999
3.440 Area in hectares
150.000 Length (PERV) metres
1.000 Gradient (%)
.500 Per cent Impervious
150.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.055 .000 .040 .000 c.m/s
.278 .859 .280 C perv/imperv/total
15 ADD RUNOFF .055 .055 .040 .000 c.m/s
11 CHANNEL
.300 Base Width =
3.000 Left bank slope 1:
3.000 Right bank slope 1:
.030 Manning's "n"
.500 O/a Depth in metres
1.000 Select Grade in %
Depth = .129 metres
Velocity = .616 m/sec
Flow Capacity = 1.222 c.m/s
Critical depth = .106 metres
9 ROUTE
400.000 Conduit Length
.492 Supply X-factor <.5
487.040 Supply K-lag (sec)
.500 Beta weighting factor
300.000 Routing timestep
1 No. of sub-reaches
.055 .055 .053 .000 c.m/s
16 NEXT LINK .055 .053 .053 .000 c.m/s
35 COMMENT
1 line(s) of comment
*** EXISTING RESIDENTIAL - DRAINAGE AREA WT ***
4 CATCHMENT
1.000 ID No.6 99999
10.840 Area in hectares
300.000 Length (PERV) metres
1.000 Gradient (%)
25.000 Per cent Impervious
300.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.515 .053 .053 .000 c.m/s
.278 .884 .429 C perv/imperv/total
15 ADD RUNOFF .515 .525 .053 .000 c.m/s
11 CHANNEL
.300 Base Width =
3.000 Left bank slope 1:
3.000 Right bank slope 1:
.030 Manning's "n"
.500 O/a Depth in metres
1.000 Select Grade in %
Depth = .352 metres
Velocity = 1.098 m/sec
Flow Capacity = 1.222 c.m/s
Critical depth = .317 metres
9 ROUTE
200.000 Conduit Length
.463 Supply X-factor <.5
136.564 Supply K-lag (sec)
.500 Beta weighting factor
120.000 Routing timestep
1 No. of sub-reaches
.515 .525 .476 .000 c.m/s
16 NEXT LINK .515 .476 .476 .000 c.m/s
35 COMMENT
1 line(s) of comment
*** MEADOW HEIGHTS - DRAINAGE AREA MH ***
4 CATCHMENT
1.000 ID No.6 99999
29.250 Area in hectares
500.000 Length (PERV) metres
2.000 Gradient (%)
35.700 Per cent Impervious
500.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
1.941 .476 .476 .000 c.m/s
.278 .882 .493 C perv/imperv/total
15 ADD RUNOFF 1.941 2.416 .476 .000 c.m/s
27 HYDROGRAPH DISPLAY
5 is # of Hyeto/Hydrograph chosen
Volume = .9127035E+04 c.m
8 PIPE
.500 Minimum velocity m/sec
2.920 Maximum velocity m/sec
.013 Pipe Manning's "n"
1.350 Diameter in metres
.500 Select Grade in %
Depth = .741 metres
Velocity = 3.000 m/sec
Pipe Capacity = 4.134 c.m/s
Critical depth= .829 metres
9 ROUTE
500.000 Conduit Length
.424 Supply X-factor <.5
124.986 Supply K-lag (sec)
.500 Beta weighting factor
120.000 Routing timestep
1 No. of sub-reaches
1.941 2.416 2.180 .000 c.m/s
22 FILE HYDROGRAPH
2 l=READ; 2=WRITE
7 MEADOWS .5YR is Filename
3 l=Overland; 2=Inflow; 3=Outflow; 4=Temp'ary
1.844 .428 2.086 2.086 c.m/s
1.941 2.416 2.180 .000 c.m/s
17 COMBINE
0 Junction Node No.
1.941 2.416 2.180 2.180 c.m/s
14 START
1 l=Zero; 2=Define
35 COMMENT
1 line(s) of comment
*** ROSEDALE - DRAINAGE AREA RD ***
4 CATCHMENT
1.000 ID No.6 99999
12.770 Area in hectares
400.000 Length (PERV) metres
2.000 Gradient (%)
70.000 Per cent Impervious
400.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
1.643 .000 2.180 2.180 c.m/s
.278 .883 .702 C perv/imperv/total
15 ADD RUNOFF 1.643 1.643 2.180 2.180 c.m/s
27 HYDROGRAPH DISPLAY
5 is # of Hyeto/Hydrograph chosen
Volume = .4079595E+04 c.m
35 COMMENT
1 line(s) of comment
*** SITE - EX FLOWS OF 147 L/S DURING 5 YR ***
10 POND
9 Depth - Discharge - Volume sets
174.850 .000 .0
175.350 .0310 1713.0
175.600 .0400 2746.0
175.760 .0800 3467.0
175.850 .0829 3893.0
176.350 .0830 6538.0
176.650 .0831 8354.0
176.750 .233 8999.0

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Stormwater Management Plan

Rosedale Subdivision – City of Port Colborne

	176.850	.473	9663.0	.460	Supply X-factor <.5				
	Peak Outflow	=	.072 c.m/s	130.387	Supply K-lag (sec)				
	Maximum Depth	=	175.729 metres	.500	Beta weighting factor				
	Maximum Storage	=	3327. c.m	120.000	Routing timestep				
	1.643	1.643	.072	2.180 c.m/s	1	No. of sub-reaches			
22	FILE HYDROGRAPH				1	.613	.632	.579	.000 c.m/s
	2	1=READ: 2=WRITE			16	NEXT LINK			
	7	ROSEDAL .5YR is Filename				.613	.579	.579	.000 c.m/s
	3	1=Overland: 2=Inflow: 3=Outflow: 4=Temp'ary			35	COMMENT			
	1.844	.428	2.086	2.086 c.m/s	1	line(s) of comment			
	1.643	1.643	.072	2.180 c.m/s		*** MEADOW HEIGHTS - DRAINAGE AREA MH ***			
17	COMBINE				4	CATCHMENT			
	0	Junction Node No.				1.000	ID No.6 99999		
	1.643	1.643	.072	2.206 c.m/s		29.250	Area in hectares		
35	COMMENT					500.000	Length (PERV) metres		
	1	line(s) of comment				2.000	Gradient (%)		
	*** OVERALL - EX FLOWS OF 2224 L/S DURING 5 YR ***					35.700	Per cent Impervious		
18	CONFLUENCE					500.000	Length (IMPERV)		
	0	Junction Node No.				.000	%Imp. with Zero Dpth		
	1.643	2.206	.072	.000 c.m/s		1	Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat		
14	START					.250	Manning "n"		
	1	1=Zero; 2=Define				77.000	SCS Curve No or C		
35	COMMENT					1.00	Ia/S Coefficient		
	3	line(s) of comment				7.587	Initial Abstraction		
	*****					1	Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv		
	* MTO 10 YEAR DESIGN STORM EVENT *					2.305	.579	.579	.000 c.m/s
	*****					.320	.898	.526	C perv/imperv/total
2	STORM				15	ADD RUNOFF			
	1	1=Chicago;2=Huff;3=User;4=Cdnlhr;5=Historic				2.305	2.884	.579	.000 c.m/s
608.845	Coefficient a				27	HYDROGRAPH DISPLAY			
.000	Constant b (min)				5	is # of Hyeto/Hydrograph chosen			
.699	Exponent c					Volume =	.1136950E+05 c.m		
.450	Fraction to peak r				8	PIPE			
240.000	Duration 6 240 min					.500	Minimum velocity m/sec		
	52.815 mm Total depth					2.920	Maximum velocity m/sec		
3	IMPERVIOUS					.013	Pipe Manning's 'n'		
	1	Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat				1.350	Diameter in metres		
.015	Manning "n"					.600	Select Grade in %		
98.000	SCS Curve No or C						Depth =	.830 metres	
.100	Ia/S Coefficient						Velocity =	3.123 m/sec	
.518	Initial Abstraction						Pipe Capacity =	4.134 c.m/s	
35	COMMENT						Critical depth=	.908 metres	
	1	line(s) of comment			9	ROUTE			
	*** FIELD - DRAINAGE AREA FX ***					500.000	Conduit Length		
4	CATCHMENT					.407	Supply X-factor <.5		
	1.000	ID No.6 99999				120.096	Supply K-lag (sec)		
	3.440	Area in hectares				.500	Beta weighting factor		
150.000	Length (PERV) metres					120.000	Routing timestep		
1.000	Gradient (%)					1	No. of sub-reaches		
.500	Per cent Impervious					2.305	2.884	2.637	.000 c.m/s
150.000	Length (IMPERV)				16	NEXT LINK			
.000	%Imp. with Zero Dpth					2.305	2.637	2.637	.000 c.m/s
1	Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat				35	COMMENT			
.250	Manning "n"					3	line(s) of comment		
77.000	SCS Curve No or C					** DIVERSION OF 5 YEAR FLOWS + 15% TO STORM SEWER **			
.100	Ia/S Coefficient					** 2180L/S + 15% = 2507L/S **			
7.587	Initial Abstraction					** ALL FLOWS GREATER THAN THE 5YR+15% DIRECTED TO WETPOND **			
1	Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv				12	DIVERT			
.079	.000	.072	.000 c.m/s			1	U/S Node No.6 99999		
.320	.878	.322	C perv/imperv/total			2.507	Threshold Discharge		
15	ADD RUNOFF					2.507	Max. Outflow reqd.		
.079	.079	.072	.000 c.m/s				Qmax & Vol.Diverted =	.130 c.m/s	78.1 c.m
11	CHANNEL						No flow diverted		
.300	Base Width =					2.305	2.637	2.507	.000 c.m/s
3.000	Left bank slope 1:				17	COMBINE			
3.000	Right bank slope 1:					1	Junction Node No.		
.030	Manning's "n"					2.305	2.637	2.507	2.507 c.m/s
.500	O/a Depth in metres				22	FILE HYDROGRAPH			
1.000	Select Grade in %					1	1=READ: 2=WRITE		
Depth =	.154 metres					12	DIV00001.010 is Filename		
Velocity =	.679 m/sec					2	1=Overland: 2=Inflow: 3=Outflow: 4=Temp'ary		
Flow Capacity =	1.222 c.m/s						2.305	.130	2.507
Critical depth =	.129 metres				35	COMMENT			
9	ROUTE					1	line(s) of comment		
400.000	Conduit Length					4	*** ROSEDAL - DRAINAGE AREA FUT ***		
.491	Supply X-factor <.5					1.000	ID No.6 99999		
441.992	Supply K-lag (sec)					12.770	Area in hectares		
.500	Beta weighting factor					400.000	Length (PERV) metres		
300.000	Routing timestep					3.000	Gradient (%)		
1	No. of sub-reaches					70.000	Per cent Impervious		
.079	.079	.077	.000 c.m/s			400.000	Length (IMPERV)		
16	NEXT LINK					.000	%Imp. with Zero Dpth		
.079	.077	.077	.000 c.m/s			1	Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat		
35	COMMENT					.250	Manning "n"		
	1	line(s) of comment				77.000	SCS Curve No or C		
	*** EXISTING RESIDENTIAL - DRAINAGE AREA WT ***					.100	Ia/S Coefficient		
4	CATCHMENT					7.587	Initial Abstraction		
	1.000	ID No.6 99999				1	Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv		
	10.840	Area in hectares				1.861	.130	2.507	2.507 c.m/s
300.000	Length (PERV) metres					.320	.893	.721	C perv/imperv/total
1.000	Gradient (%)					15	ADD RUNOFF		
25.000	Per cent Impervious					1.861	1.991	2.507	2.507 c.m/s
300.000	Length (IMPERV)								
.000	%Imp. with Zero Dpth					27	HYDROGRAPH DISPLAY		
1	Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat					5	is # of Hyeto/Hydrograph chosen		
.250	Manning "n"						Volume =	.4940556E+04 c.m	
77.000	SCS Curve No or C					35	COMMENT		
.100	Ia/S Coefficient					1	line(s) of comment		
7.587	Initial Abstraction					10	*** SITE - EX FLOWS OF 225 L/S DURING 10 YR ***		
1	Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv					9	Depth - Discharge - Volume sets		
.613	.077	.077	.000 c.m/s			174.850	.000	.0	
.320	.897	.464	C perv/imperv/total			175.350	.0310	1713.0	
15	ADD RUNOFF					175.600	.0400	2746.0	
.613	.632	.077	.000 c.m/s			175.760	.0800	3467.0	
11	CHANNEL					175.850	.0829	3893.0	
.300	Base Width =					176.350	.0830	6538.0	
3.000	Left bank slope 1:					176.650	.0831	8354.0	
3.000	Right bank slope 1:					176.750	.233	8999.0	
.030	Manning's "n"					176.850	.473	9663.0	
.500	O/a Depth in metres					Peak Outflow =	.083 c.m/s		
1.000	Select Grade in %					Maximum Depth =	175.870 metres		
Depth =	.381 metres					Maximum Storage =	4001. c.m		
Velocity =	1.150 m/sec					1.861	1.991	.083	
Flow Capacity =	1.222 c.m/s					17	COMBINE		
Critical depth =	.344 metres					1	Junction Node No.		
9	ROUTE					1.861	1.991	.083	2.540 c.m/s
200.000	Conduit Length								

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35	COMMENT	500.000	Length (PERV) metres				
1	line(s) of comment	2.000	Gradient (%)				
18	CONFLUENCE	35.700	Per cent Impervious				
1	Junction Node No.	500.000	Length (IMPERV)				
14	START	.000	%Imp. with Zero Dpth				
1	l=Zero; 2=Define	.250	Manning "n"				
35	COMMENT	77.000	SCS Curve No or C				
3	line(s) of comment	.100	Ia/S Coefficient				
	*****	7.587	Initial Abstraction				
	* MTO 25 YEAR DESIGN STORM EVENT *	1	Option 1=Triangl; 2=Rectangl; 3=SWM HYD; 4=Lin. Reserv				
	*****	2.767	.720	.720	.000	c.m/s	
2	STORM	.367	.911	.561		C perv/imperv/total	
1	l=Chicago;2=Huff;3=User;4=Cdnlhr;5=Historic	15	ADD RUNOFF	2.767	3.486	.720	.000
715.568	Coefficient a	27	HYDROGRAPH DISPLAY	5	is # of Hyeto/Hydrograph chosen		
.000	Constant b (min)	8	PIPE		Volume = .1435674E+05	c.m	
.699	Exponent c		.500	Minimum velocity	m/sec		
.450	Fraction to peak r		2.920	Maximum velocity	m/sec		
240.000	Duration δ 240 min		.013	Pipe Manning's 'n'			
	62.073 mm		1.350	Diameter in metres			
	Total depth		.600	Select Grade in %			
3	IMPERVIOUS		Depth =	.950	metres		
1	Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat		Velocity =	3.238	m/sec		
.015	Manning "n"		Pipe Capacity =	4.134	c.m/s		
98.000	SCS Curve No or C		Critical depth=	.999	metres		
.100	Ia/S Coefficient		ROUTE				
.518	Initial Abstraction	9	500.000	Conduit Length			
35	COMMENT		.377	Supply X-factor <.5			
1	line(s) of comment		115.797	Supply K-lag (sec)			
4	CATCHMENT		.500	Beta weighting factor			
1.000	ID No. δ 99999		120.000	Routing timestep			
3.440	Area in hectares		1	No. of sub-reaches			
150.000	Length (PERV) metres		2.767	3.486	3.226	.000	c.m/s
1.000	Gradient (%)		16	NEXT LINK	2.767	3.226	3.226
.500	Per cent Impervious		35	COMMENT			
150.000	Length (IMPERV)		3	line(s) of comment			
.000	%Imp. with Zero Dpth			** DIVERSION OF 5 YEAR FLOWS + 15% TO STORM SEWER **			
1	Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat			** 2180L/S + 15% = 2507L/S **			
.250	Manning "n"			** ALL FLOWS GREATER THAN THE 5YR+15% DIRECTED TO WETPOND **			
77.000	SCS Curve No or C		12	DIVERT			
.100	Ia/S Coefficient		1	U/S Node No. δ 99999			
7.587	Initial Abstraction		2.507	Threshold Discharge			
1	Option 1=Triangl; 2=Rectangl; 3=SWM HYD; 4=Lin. Reserv		2.507	Max. Outflow reqd.			
.127	.000	.083		Qmax & Vol. Diverted =	.719	c.m/s	431.6
.367	.898	.369		No flow diverted			
15	ADD RUNOFF	.127	.127	.083	.000	c.m/s	
11	CHANNEL						
.300	Base Width =						
3.000	Left bank slope 1:						
3.000	Right bank slope 1:						
.030	Manning's "n"						
.500	O/a Depth in metres						
1.000	Select Grade in %						
Depth =	.190	metres					
Velocity =	.766	m/sec					
Flow Capacity =	1.222	c.m/s					
Critical depth =	.162	metres					
9	ROUTE						
400.000	Conduit Length						
.489	Supply X-factor <.5						
391.534	Supply K-lag (sec)						
.500	Beta weighting factor						
300.000	Routing timestep						
1	No. of sub-reaches						
.127	.127	.122	.000	c.m/s			
16	NEXT LINK	.127	.122	.122	.000	c.m/s	
35	COMMENT						
1	line(s) of comment						
4	CATCHMENT						
1.000	ID No. δ 99999						
10.840	Area in hectares						
300.000	Length (PERV) metres						
1.000	Gradient (%)						
25.000	Per cent Impervious						
300.000	Length (IMPERV)						
.000	%Imp. with Zero Dpth						
1	Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat						
.250	Manning "n"						
77.000	SCS Curve No or C						
.100	Ia/S Coefficient						
7.587	Initial Abstraction						
1	Option 1=Triangl; 2=Rectangl; 3=SWM HYD; 4=Lin. Reserv						
.742	.122	.122	.000	c.m/s			
.367	.911	.503		C perv/imperv/total			
15	ADD RUNOFF	.742	.775	.122	.000	c.m/s	
11	CHANNEL						
.300	Base Width =						
3.000	Left bank slope 1:						
3.000	Right bank slope 1:						
.030	Manning's "n"						
.500	O/a Depth in metres						
1.000	Select Grade in %						
Depth =	.415	metres					
Velocity =	1.211	m/sec					
Flow Capacity =	1.222	c.m/s					
Critical depth =	.377	metres					
9	ROUTE						
200.000	Conduit Length						
.457	Supply X-factor <.5						
123.848	Supply K-lag (sec)						
.500	Beta weighting factor						
120.000	Routing timestep						
1	No. of sub-reaches						
.742	.775	.720	.000	c.m/s			
16	NEXT LINK	.742	.720	.720	.000	c.m/s	
35	COMMENT						
1	line(s) of comment						
4	CATCHMENT						
1.000	ID No. δ 99999						
29.250	Area in hectares						

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1      1      1=Chicago;2=Huff;3=User;4=Cdnlhr;5=Historic
794.298 Coefficient a
.000 Constant b (min)
.699 Exponent c
.450 Fraction to peak r
240.000 Duration 6 240 min
68.903 mm Total depth
3      IMPERVIOUS
1      1      Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.015 Manning "n"
98.000 SCS Curve No or C
.100 Ia/S Coefficient
.518 Initial Abstraction
35     COMMENT
1      1      line(s) of comment
4      4      *** FIELD - DRAINAGE AREA FX ***
CATCHMENT
1.000 ID No.6 99999
3.440 Area in hectares
150.000 Length (PERV) metres
1.000 Gradient (%)
.500 Per cent Impervious
150.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1      1      Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1      1      Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.161 .000 .083 .000 c.m/s
.397 .909 .400 C perv/imperv/total
15     ADD RUNOFF
.161 .161 .083 .000 c.m/s
11     CHANNEL
.300 Base Width =
3.000 Left bank slope 1:
3.000 Right bank slope 1:
.030 Manning's "n"
.500 O/a Depth in metres
1.000 Select Grade in %
Depth = .211 metres
Velocity = .814 m/sec
Flow Capacity = 1.222 c.m/s
Critical depth = .182 metres
9      ROUTE
400.000 Conduit Length
.488 Supply X-factor <.5
368.744 Supply K-lag (sec)
.500 Beta weighting factor
300.000 Routing timestep
1      1      No. of sub-reaches
.161 .161 .154 .000 c.m/s
16     NEXT LINK
.161 .154 .154 .000 c.m/s
35     COMMENT
1      1      line(s) of comment
4      4      *** EXISTING RESIDENTIAL - DRAINAGE AREA WT ***
CATCHMENT
1.000 ID No.6 99999
10.840 Area in hectares
300.000 Length (PERV) metres
1.000 Gradient (%)
25.000 Per cent Impervious
300.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1      1      Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1      1      Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.841 .154 .154 .000 c.m/s
.397 .917 .527 C perv/imperv/total
15     ADD RUNOFF
.841 .888 .154 .000 c.m/s
11     CHANNEL
.300 Base Width =
3.000 Left bank slope 1:
3.000 Right bank slope 1:
.030 Manning's "n"
.500 O/a Depth in metres
1.000 Select Grade in %
Depth = .439 metres
Velocity = 1.253 m/sec
Flow Capacity = 1.222 c.m/s
Critical depth = .400 metres
9      ROUTE
200.000 Conduit Length
.455 Supply X-factor <.5
119.694 Supply K-lag (sec)
.500 Beta weighting factor
120.000 Routing timestep
1      1      No. of sub-reaches
.841 .888 .829 .000 c.m/s
16     NEXT LINK
.841 .829 .829 .000 c.m/s
35     COMMENT
1      1      line(s) of comment
4      4      *** MEADOW HEIGHTS - DRAINAGE AREA MH ***
CATCHMENT
1.000 ID No.6 99999
29.250 Area in hectares
500.000 Length (PERV) metres
2.000 Gradient (%)
35.700 Per cent Impervious
500.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1      1      Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1      1      Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
3.111 .829 .829 .000 c.m/s
.397 .919 .584 C perv/imperv/total
15     ADD RUNOFF
3.111 3.940 .829 .000 c.m/s
HYDROGRAPH DISPLAY
5      5      is # of Hyeto/Hydrograph chosen
Volume = .1664438E+05 c.m
PIPE
.500 Minimum velocity m/sec
2.920 Maximum velocity m/sec
.013 Pipe Manning's 'n'
1.350 Diameter in metres
.600 Select Grade in %
Depth = 1.053 metres
Velocity = 3.288 m/sec
Pipe Capacity = 4.134 c.m/s
Critical depth= 1.060 metres
9      ROUTE
500.000 Conduit Length
.344 Supply X-factor <.5
114.065 Supply K-lag (sec)
.500 Beta weighting factor
120.000 Routing timestep
1      1      No. of sub-reaches
3.111 3.940 3.669 .000 c.m/s
16     NEXT LINK
3.111 3.669 3.669 .000 c.m/s
35     COMMENT
3      3      line(s) of comment
** DIVERSION OF 5 YEAR FLOWS + 15% TO STORM SEWER **
** 2180L/S + 15% = 2507L/S **
** ALL FLOWS GREATER THAN THE 5YR+15% DIRECTED TO WETPOND **
DIVERT
1      1      U/S Node No.6 99999
2.507 Threshold Discharge
2.507 Max. Outflow reqd.
Qmax & Vol.Diverted = 1.162 c.m/s 720.0 c.m
No flow diverted
3.111 3.669 2.507 .000 c.m/s
17     COMBINE
1      1      Junction Node No.
3.111 3.669 2.507 2.507 c.m/s
22     FILE HYDROGRAPH
1      1      1=READ; 2=WRITE
12     DIV0001.050 is Filename
2      2      1=Overland; 2=Inflow; 3=Outflow; 4=Temp'ary
3.111 1.162 2.507 2.507 c.m/s
35     COMMENT
1      1      line(s) of comment
4      4      *** ROSEDALE - DRAINAGE AREA FUT ***
CATCHMENT
1.000 ID No.6 99999
12.770 Area in hectares
400.000 Length (PERV) metres
3.000 Gradient (%)
70.000 Per cent Impervious
400.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1      1      Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1      1      Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
2.448 1.162 2.507 2.507 c.m/s
.398 .903 .752 C perv/imperv/total
15     ADD RUNOFF
2.448 3.610 2.507 2.507 c.m/s
27     HYDROGRAPH DISPLAY
5      5      is # of Hyeto/Hydrograph chosen
Volume = .7332710E+04 c.m
35     COMMENT
1      1      line(s) of comment
10     10     POND
9      9      Depth - Discharge - Volume sets
174.850 .000 .0
175.350 .0310 1713.0
175.600 .0400 2746.0
175.760 .0800 3467.0
175.850 .0829 3893.0
176.350 .0830 6538.0
176.650 .0831 8354.0
176.750 .233 8999.0
176.850 .473 9663.0
Peak Outflow = .083 c.m/s
Maximum Depth = 176.295 metres
Maximum Storage = 6247. c.m
2.448 3.610 .083 2.507 c.m/s
17     COMBINE
1      1      Junction Node No.
2.448 3.610 .083 2.590 c.m/s
35     COMMENT
1      1      line(s) of comment
18     18     *** OVERALL - EX FLOWS OF 3824 L/S DURING 50 YR ***
CONFLUENCE
1      1      Junction Node No.
2.448 2.590 .083 .000 c.m/s
14     START
1      1      1=Zero; 2=Define
35     35     COMMENT
3      3      line(s) of comment
*****
* MTO 100 YEAR DESIGN STORM EVENT *
*****
2      2      STORM
1      1      1=Chicago;2=Huff;3=User;4=Cdnlhr;5=Historic
871.279 Coefficient a
.000 Constant b (min)
.699 Exponent c
.450 Fraction to peak r
240.000 Duration 6 240 min
75.581 mm Total depth
3      3      IMPERVIOUS
1      1      Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.015 Manning "n"
98.000 SCS Curve No or C
.100 Ia/S Coefficient
.518 Initial Abstraction
35     35     COMMENT

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1 line(s) of comment
*** FIELD - DRAINAGE AREA FX ***
4 CATCHMENT
1.000 ID No.6 99999
3.440 Area in hectares
150.000 Length (PERV) metres
1.000 Gradient (%)
.500 Per cent Impervious
150.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.196 .000 .083 .000 c.m/s
.425 .917 .427 C perv/imperv/total
15 ADD RUNOFF
.196 .196 .083 .000 c.m/s
11 CHANNEL
.300 Base Width =
3.000 Left bank slope 1:
3.000 Right bank slope 1:
.030 Manning's "n"
.500 O/a Depth in metres
1.000 Select Grade in %
Depth = .231 metres
Velocity = .856 m/sec
Flow Capacity = 1.222 c.m/s
Critical depth = .200 metres
9 ROUTE
400.000 Conduit Length
.487 Supply X-factor <.5
350.564 Supply K-lag (sec)
.500 Beta weighting factor
300.000 Routing timestep
1 No. of sub-reaches
.196 .196 .186 .000 c.m/s
16 NEXT LINK
.196 .186 .186 .000 c.m/s
35 COMMENT
1 line(s) of comment
*** EXISTING RESIDENTIAL - DRAINAGE AREA WT ***
4 CATCHMENT
1.000 ID No.6 99999
10.840 Area in hectares
300.000 Length (PERV) metres
1.000 Gradient (%)
25.000 Per cent Impervious
300.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
.924 .186 .186 .000 c.m/s
.425 .922 .549 C perv/imperv/total
15 ADD RUNOFF
.924 .988 .186 .000 c.m/s
11 CHANNEL
.300 Base Width =
3.000 Left bank slope 1:
3.000 Right bank slope 1:
.030 Manning's "n"
.500 O/a Depth in metres
1.000 Select Grade in %
Depth = .458 metres
Velocity = 1.287 m/sec
Flow Capacity = 1.222 c.m/s
Critical depth = .420 metres
9 ROUTE
200.000 Conduit Length
.453 Supply X-factor <.5
116.540 Supply K-lag (sec)
.500 Beta weighting factor
120.000 Routing timestep
1 No. of sub-reaches
.924 .988 .929 .000 c.m/s
16 NEXT LINK
.924 .929 .929 .000 c.m/s
35 COMMENT
1 line(s) of comment
*** MEADOW HEIGHTS - DRAINAGE AREA MH ***
4 CATCHMENT
1.000 ID No.6 99999
29.250 Area in hectares
500.000 Length (PERV) metres
2.000 Gradient (%)
35.700 Per cent Impervious
500.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
3.453 .929 .929 .000 c.m/s
.425 .926 .604 C perv/imperv/total
15 ADD RUNOFF
3.453 4.381 .929 .000 c.m/s
27 HYDROGRAPH DISPLAY
5 is # of Hyeto/Hydrograph chosen
Volume = .1895466E+05 c.m
8 PIPE
.500 Minimum velocity m/sec
2.920 Maximum velocity m/sec
.013 Pipe Manning's 'n'
1.350 Diameter in metres
.600 Select Grade in %
Surcharged HGL= .674 %
Velocity = 3.061 m/sec
Pipe Capacity = 4.134 c.m/s
Critical depth= 1.113 metres
9 ROUTE
500.000 Conduit Length
.500 Supply X-factor <.5
.000 Supply K-lag (sec)
.500 Beta weighting factor
600.000 Routing timestep
1 No. of sub-reaches
3.453 4.381 4.381 .000 c.m/s
16 NEXT LINK
3.453 4.381 4.381 .000 c.m/s
35 COMMENT
3 line(s) of comment
** DIVERSION OF 5 YEAR FLOWS + 15% TO STORM SEWER **
** 2180L/S + 15% = 2507L/S **
** ALL FLOWS GREATER THAN THE 5YR+15% DIRECTED TO WETPOND **
12 DIVERT
1 U/S Node No.6 99999
2.507 Threshold Discharge
2.507 Max. Outflow reqd.
Qmax & Vol.Diverted = 1.874 c.m/s 1354.0 c.m
No flow diverted
3.453 4.381 2.507 .000 c.m/s
17 COMBINE
1 Junction Node No.
3.453 4.381 2.507 2.507 c.m/s
22 FILE HYDROGRAPH
1 1=READ; 2=WRITE
12 DIV0001.100 is Filename
2 1=Overland; 2=Inflow; 3=Outflow; 4=Temp'ary
3.453 1.874 2.507 2.507 c.m/s
35 COMMENT
1 line(s) of comment
*** ROSEDALE - DRAINAGE AREA FUT ***
4 CATCHMENT
1.000 ID No.6 99999
12.770 Area in hectares
400.000 Length (PERV) metres
3.000 Gradient (%)
70.000 Per cent Impervious
400.000 Length (IMPERV)
.000 %Imp. with Zero Dpth
1 Option 1=SCS CN/C; 2=Horton; 3=Green-Ampt; 4=Repeat
.250 Manning "n"
77.000 SCS Curve No or C
.100 Ia/S Coefficient
7.587 Initial Abstraction
1 Option 1=Trianglr; 2=Rectanglr; 3=SWM HYD; 4=Lin. Reserv
2.688 1.874 2.507 2.507 c.m/s
.425 .904 .760 C perv/imperv/total
15 ADD RUNOFF
2.688 4.562 2.507 2.507 c.m/s
27 HYDROGRAPH DISPLAY
5 is # of Hyeto/Hydrograph chosen
Volume = .8693769E+04 c.m
35 COMMENT
1 line(s) of comment
*** SITE - EX FLOWS OF 550 L/S DURING 100 YR ***
10 POND
9 Depth - Discharge - Volume sets
174.850 .000 .0
175.350 .0310 1713.0
175.600 .0400 2746.0
175.760 .0800 3467.0
175.850 .0829 3893.0
176.350 .0830 6538.0
176.650 .0831 8354.0
176.750 .233 8999.0
176.850 .473 9663.0
Peak Outflow = .083 c.m/s
Maximum Depth = 176.520 metres
Maximum Storage = 7568. c.m
2.688 4.562 .083 2.507 c.m/s
17 COMBINE
1 Junction Node No.
2.688 4.562 .083 2.589 c.m/s
35 COMMENT
1 line(s) of comment
*** OVERALL - EX FLOWS OF 4585 L/S DURING 100 YR ***
18 CONFLUENCE
1 Junction Node No.
2.688 2.589 .083 .000 c.m/s
20 MANUAL

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